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(54) Operation mode transition of an automated transmission

(57) A degraded mode of operation (Figure 7) for a partially automated mechanical transmission system having a splitter-type mechanical transmission with a splitter section automatically shifted in only certain ratios (ninth/tenth). Upon sensing certain system faults when in this automatic splitter shifting mode, the splitter section is retained, as is, until main section neutral can be confirmed, at which time the splitter section is returned to manual control for all transmission ratios.

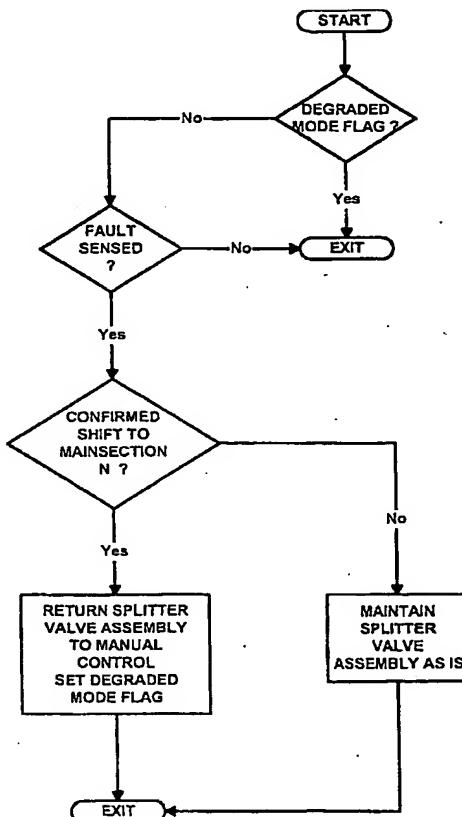


FIG. 7

Description**BACKGROUND OF THE INVENTION****RELATED APPLICATIONS**

This application is related to the following copending U.S. applications, all assigned to EATON CORPORATION, the assignee of this application:

Serial No. 08/439,908

Filed: 12/05/95

Title: AUTOMATIC AND MANUAL SPLITTER SHIFTING CONTROL VALVE ASSEMBLY

Serial No. 08/649,829

Filed: 30/04/96

Title: SYNCHRONIZING AND GEAR ENGAGEMENT SENSING LOGIC FOR AUTOMATED MECHANICAL TRANSMISSION SYSTEMS

Serial No. 795,918 [96-TRN-113]

Filed: 05/02/97

Title: AUTOMATED TRANSMISSION SYSTEM POWER-DOWN

Serial No. 796,001 [96-TRN-114]

Filed: 05/02/97

Title: SENSING MANUAL SHIFT INTO AUTOMATED UPPER RATIOS

Serial No. 796,006 [96-TRN-116]

Filed: 05/02/97

Title: AUTOMODE-TO-NEUTRAL LOGIC

Serial No. 795,616 [96-TRN-117]

Filed: 05/02/97

Title: ANTI-HUNT LOGIC

Serial No. 795,615 [96-TRN-119]

Filed: 05/02/97

Title: DISENGAGEMENT CONFIRMATION

Serial No. 790,210 [96-TRN-121]

Filed: 05/02/97

Title: ENGAGEMENT OF GEAR RATIO CONFIRMATION

FIELD OF THE INVENTION

The present invention relates to a fault-tolerant logic

for a partially automated mechanical transmission system having automated splitter shifting in at least one main section ratio position.

5 DESCRIPTION OF THE PRIOR ART

Partially automated vehicular transmission systems requiring manual shifting in the lower ratios and having a control for automated shifting in the upper ratios are

10 known in the prior art, as may be seen by reference to U.S. Patents No. 4,722,248; 4,850,236; 5,038,627; 5,393,276; 5,393,277 and 5,498,195.

Splitter and combined range and splitter-type compound vehicular transmissions requiring manual splitter shifting are well known in the prior art, as may be seen by reference to U.S. Patents No. 3,799,002; 4,754,665; 4,974,468; 5,000,060; 5,370,013 and 5,390,561. Transmissions with automatic splitter shifting are known in the prior art, as may be seen by reference to U.S. Patent No. 5,435,212.

Fault-tolerant and limp-home routines for automated mechanical transmission systems are known in the prior art, as may be seen by reference to U.S. Patents No. 5,109,721 and 5,157,607.

25 SUMMARY OF THE INVENTION

In accordance with the present invention, a new and improved control system/method for an automated mechanical transmission system having automated splitter shift in certain ratios only and manual splitter shifting in other ratios and an improved fault-tolerant degraded mode of operation is provided.

The foregoing is accomplished by providing a logic which, in the event of faults which will adversely affect automatic splitter shifting, maintains the automated splitter shifting mechanism engaged in the currently engaged splitter ratio until a manual shift into neutral is sensed, at which time the splitter mechanism is returned to manual control.

Accordingly, it is an object of the present invention to provide a new and improved fault-tolerant degraded mode of operation for a partially automated mechanical transmission system having manually and automatically controlled splitter shifting.

This and other objects and advantages of the present invention will become apparent from a reading of the following description of the preferred embodiment taken in connection with the attached drawings.

50 BRIEF DESCRIPTION OF THE DRAWINGS

Figures 1 and 1A are sectional views of a typical splitter or combined splitter and range-type compound transmission.

Figure 2 is a schematic illustration of the manual shift pattern and ratio steps for the transmission of Figures 1 and 1A.

Figure 3 is a schematic illustration of a partially automated vehicular mechanical transmission system having both manual and automatic splitter shifting and utilizing the control of the present invention.

Figure 4 is a valve table for the control valve assembly utilized in the system of Figure 3.

Figure 5 is a schematic illustration, similar to Figure 2, of the shift pattern and ratio steps for the transmission system of Figure 3.

Figure 6 is a graphical representation of the disengagement confirmation logic of the system of Figure 3.

Figure 7 is a schematic illustration, in flow chart format, of the fault-tolerant degraded mode of operation logic of the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Figures 1, 1A and 2 illustrate a typical combined splitter and range-type compound mechanical transmission 10 of the type advantageously utilized in connection with the control of the present invention.

Transmission 10 comprises a main transmission section 12 connected in series with an auxiliary transmission section 14 having both range and splitter-type gearing. Typically, transmission 10 is housed within a single multi-piece housing 16 and includes an input shaft 18 driven by a prime mover (such as a diesel engine) through a selectively disengaged, normally engaged friction master clutch.

In the main transmission section 12, the input shaft 18 carries an input gear 20 for driving at least one countershaft assembly 22. Preferably, as is well known in the prior art and as is illustrated in U.S. Patents No. 3,105,395 and 3,335,616, input gear 20 simultaneously drives a plurality of substantially identical main section countershaft assemblies at substantially identical rotational speeds. Each of the main section countershaft assemblies comprises a main section countershaft 24 supported by bearings 26 and 28 in housing 16 and is provided with main section countershaft gears 30, 32, 34, 36 and 38 fixed thereto. A plurality of main section drive or main shaft gears 40, 42 and 44 surround the transmission main shaft 46 and are selectively clutchable, one at a time, to the main shaft 46 for rotation therewith by sliding clutch collars 48 and 50, as is well known in the art. Clutch collar 48 may also be utilized to clutch input gear 20 to the main shaft 46 to provide a direct drive relationship between the input shaft 18 and the main shaft 46. Preferably, each of the main section main shaft gears encircles the main shaft 46 and is in continuous meshing engagement with and is floatingly supported by the associated countershaft gear groups, which mounting means and special advantages resulting therefrom are explained in greater detail in aforementioned U.S. Patents No. 3,105,395 and 3,335,616. Typically, clutch collars 48 and 50 are axially positioned by means of shift forks or yokes 52 and 54, respectively, associated with a shift bar housing assembly 56 of the

type illustrated in U.S. Patents No. 4,920,815 and 5,000,060. Clutch collars 48 and 50 are, in the preferred embodiment, of the well-known, non-synchronized, double-acting jaw clutch type.

- 5 Main section main shaft gear 44 is the reverse gear and is in continuous meshing engagement with counter-shaft gears 38 by means of conventional intermediate idler gears 57 (see Figure 1A). Main section counter-shaft gear 32 is provided for powering power takeoff devices and the like. Jaw clutches 48 and 50 are 3-position clutches in that they may be positioned in a centered axially non-displaced, non-engaged position as illustrated or in a fully rightwardly engaged or fully leftwardly engaged position.
- 10 Auxiliary transmission section 14 is connected in series with main transmission section 12 and is of the 3-layer, 4-speed combined splitter/range type, as illustrated in above-mentioned U.S. Patent No. 4,754,665. Main shaft 46 extends into the auxiliary section 14 and is journaled in the inward end of the output shaft 58 which extends from the rearward end of the transmission.
- 15 Auxiliary transmission section 14 includes, in the preferred embodiment thereof, a plurality of substantially identical auxiliary countershaft assemblies 60 (see Figure 1A), each comprising an auxiliary countershaft 62 supported by bearings 64 and 66 in housing 16 and carrying three auxiliary section countershaft gears 68, 70 and 72 fixed for rotation therewith. Auxiliary counter-shaft gears 68 are constantly meshed with and support auxiliary section splitter gear 74. Auxiliary countershaft gears 70 are constantly meshed with and support auxiliary section splitter/range gear 76 which surrounds the output shaft 58 at the end thereof adjacent the coaxial inner end of main shaft 46. Auxiliary section countershaft gears 72 constantly mesh with and support auxiliary section range gear 78, which surrounds the output shaft 58. Accordingly, auxiliary section countershaft gears 68 and splitter gear 74 define a first gear layer, auxiliary section countershaft gears 70 and splitter/range gear 76 define a second gear layer and auxiliary section countershaft gears 72 and range gear 78 define a third layer, or gear group, of the combined splitter and range-type auxiliary transmission section 14.
- 20 A sliding 2-position jaw clutch collar 80 is utilized to selectively couple either the splitter gear 74 or the splitter/range gear 76 to the main shaft 46, while a 2-position synchronized clutch assembly 82 is utilized to selectively couple the splitter/range gear 76 or the range gear 78 to the output shaft 58.
- 25 The splitter jaw clutch 80 is a 2-position clutch assembly which may be selectively positioned in the rightwardmost or leftwardmost positions for engaging either gear 76 or gear 74, respectively, to the main shaft 46.
- 30 Splitter jaw clutch 80 is axially positioned by means of a shift fork 84 controlled by a 2-position piston actuator 86, which normally is operable by a driver selection switch such as a button or the like on the shift knob, as
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is known in the prior art. Two-position synchronized range clutch assembly 82 is also a 2-position clutch which may be selectively positioned in either the rightwardmost or leftwardmost positions thereof for selectively clutching either gear 78 or 76, respectively, to output shaft 58. Clutch assembly 82 is positioned by means of a shift fork 88 operated by means of a 2-position piston device 90, the actuation and control of which is described in greater detail in aforementioned U.S. Patent No. 4,974,468.

As may be seen by reference to Figures 1-2, by selectively axially positioning both the splitter clutch 80 and the range clutch 82 in the forward and rearward axial positions thereof, four distinct ratios of main shaft rotation to output shaft rotation may be provided. Accordingly, auxiliary transmission section 14 is a 3-layer auxiliary section of the combined range and splitter type providing four selectable speeds or drive ratios between the input (main shaft 46) and output (output shaft 58) thereof. The main section 12 provides a reverse and three potentially selectable forward speeds. However, one of the selectable main section forward gear ratios, the low speed gear ratios associated with main shaft gear 42, is not utilized in the high range. Thus, transmission 10 is properly designated as a "(2+1)x(2x2)" type transmission providing nine or ten selectable forward speeds, depending upon the desirability and practicality of splitting the low gear ratio.

While clutch 82 (the range clutch) should be a synchronized clutch, double-acting clutch collar 80 (the splitter clutch) is not required to be synchronized. The shift pattern for manually shifting transmission 10 is schematically illustrated in Figure 2. Divisions in the vertical direction at each gear lever position signify splitter shifts, while movement in the horizontal direction from the 3/4 and 5/6 leg of the H pattern to the 7/8 and 9/10 leg of the H pattern signifies a shift from the low range to the high range of the transmission. As discussed above, manual splitter shifting is accomplished in the usual manner by means of a vehicle operator-actuated splitter button or the like, usually a button located at the shift lever knob, while operation of the range clutch shifting assembly is an automatic response to movement of the gear shift lever between the central and rightward-most legs of the shift pattern, as illustrated in Figure 2. Range shift devices of this general type are known in the prior art and may be seen by reference to U.S. Patents No. 3,429,202; 4,455,883; 4,561,325 and 4,663,725. Manually operated splitter and range shift actuators are known in the prior art and may be seen by reference to U.S. Patents No. 5,193,410; 5,199,314 and 5,329,826.

A partially automated vehicular mechanical transmission system 92 utilizing the control system of the present invention is illustrated in Figure 3. Partially automated system 92 is of the type requiring manual shifting in the lower gear ratios (first through eighth) and, after initial manual selection of one of the upper two ra-

tios, providing automatic shifting in the upper gear ratios (ninth and tenth), as described in aforementioned U.S. Patents No. 4,722,248; 4,850,236; 5,038,027 and 5,393,276. The shift pattern for partially automated operation of the system 92 is schematically illustrated in Figure 5.

The system includes a splitter control valve assembly 94 and a prime mover (such as diesel engine 96) driving the input shaft 18 of transmission 10 through a master friction clutch 98. The transmission 10 includes a shift lever 100 having a shift knob 102, which is associated with the shift bar housing 56 for manually shifting main section 12 and the range clutch 82 of auxiliary section 14.

15 A manually operated splitter valve 104, having a selector lever or button 106, is provided, usually on or integral with the shift knob, for manually shifting the splitter clutch 80. Splitter valve 104 is a 2-position, 3-way manually operated valve effective to selectively connect a first pilot conduit 108 to exhaust ("Ex") or to pilot pressure, respectively, to manually select either the high or low splitter ratio. The pilot pressure may be equal to supply pressure ("S") or to a lower value. In a typical on-board pneumatic system, supply is filtered, regulated air at about 60 to 80 psi.

20 The first pilot conduit 108 may fluidly communicate with a second pilot conduit 110 in series through the control valve assembly 94 of the present invention. The second pilot conduit 110 is effective to act on a 2-position, 3-way pilot valve 112, which is effective to normally vent or selectively pressurize a control chamber 114 of the splitter piston/cylinder actuator assembly 86. Chamber 114 is exposed to the larger area face 116 of a differential area piston 118 having a smaller area face 120 constantly exposed to supply pressure in biasing chamber 122. As is known, a spring may be utilized in place of or in combination with smaller area piston face 120 to bias piston 118 rightwardly, as seen in Figure 3.

25 As may be seen, when pilot conduit 110 is exhausted, pilot valve 112 will connect control chamber 114 to exhaust, and supply pressure acting on smaller area face 120 will cause shift fork 84 to move splitter clutch 80 to engage gear 76 for the low splitter ratio, and when pilot conduit 110 is pressurized, valve 112 will move against a bias to a position for pressurizing control chamber 114, causing the piston 118 to move leftwardly to cause splitter clutch 80 to engage gear 74 for the high splitter ratio.

30 Except for interposing the control valve assembly 94 in series between pilot conduits 108 and 110, the above-described components are structurally and functionally equivalent to components utilized to shift the manually shifted transmission of Figures 1, 1A and 2.

35 To provide the partially automated operation of system 92, a controller 124, preferably a microprocessor-based controller, is provided for receiving input signals 126 and for processing same according to predetermined logic rules to issue command output signals 128

to various system actuators, such as an engine fuel control 130 and a solenoid driver and fault detection unit 132. Controllers of this type may be seen by reference to U.S. Patents No. 4,361,060 and 4,595,986. The program for controller 124 is stored on a computerusable medium such as a floppy disk, hard drive, CD-rom, tape or other external or internal storage medium.

Sensors for sensing engine speed (ES) and/or input shaft speed (IS) and output shaft speed (OS) may be provided, as well as sensors for sensing engine fueling THL and solenoid faults SF, all of which provide input signals indicative thereof to the controller 124. With the clutch 98 engaged, input shaft speed may be assumed to equal engine speed.

As is known, the engine 96 may have a built-in controller 96A and/or may communicate with controller 124 by an electronic data link of the type conforming to SAE J-1922, SAE J-1939, ISO 11898 or the like. All or a portion of controller 124 may be defined by hardware and/or software associated with engine controller 96A. A sensor may be provided for providing a signal (GR) indicative of engaged gear ratio or gear ratio may be calculated and confirmed by dividing input shaft speed or engine speed by output shaft speed ($GR = ((IS = ES)/OS \mp \text{error})$).

The control valve assembly 94 of the present invention is interposed in series between the standard manual splitter shift selection valve 104 and the standard pilot valve 112/splitter actuator 86 and is operated in response to command output signals from controller 124. The assembly includes, in series, a first 2-position, 3-way solenoid-controlled valve 134 and a second 2-position, 3-way solenoid-controlled valve 136 and a solenoid driver and fault detection unit 132 operating in response to command output signals from the controller.

Valve 134 has an inlet 138 connected to pilot conduit 108 and two outlets 140 (connected to one inlet 142 of valve 136) and 144 (connected to exhaust). Valve 134 has a first normal or default position wherein inlet 138 is connected to outlet 140, and thus, to inlet 142 of valve 136, while outlet 144 of valve 134 is blocked. Valve 134 has a second or actuated position upon energizing the first solenoid S#1 wherein outlet 140 is connected to exhaust at outlet 144 and inlet 138 is blocked.

Valve 136 has two inlets 142 (connected to the outlet 140 of valve 134) and 146 (connected to the source of pressurized fluid) and an outlet 148 connected to the second pilot conduit 110 controlling the pilot valve 112. Valve 136 has a first normal or default position wherein inlet 142 is connected to outlet 148 and the inlet 146 from source pressure is blocked, and a second actuated position upon energizing the second solenoid S#2 wherein inlet 142 is blocked and source pressure at inlet 146 communicates with outlet 148 and pilot conduit 110.

The valve table for operation of the solenoid-operated valves is set forth in Figure 4.

The controller 124 senses a manual splitter operation mode by sensing a shift bar condition GR other than

AUTO (see Figure 5). In this mode (i.e., gear ratios 1-8), the solenoid driver is commanded to deenergize both of the solenoids, and the valves 134 and 136 will assume the default positions thereof. Pilot conduit 108 will communicate with pilot conduit 110 through the valves 134 and 136, and the actuator 86 will be under the manual control of selector valve 104.

AUTO or not-AUTO mode conditions may be sensed by position sensors or by processing the ES and OS signals according to predetermined logic rules.

Upon sensing a manual shift to the AUTO position, the controller will cause the solenoid driver 132 to energize the first solenoid S#1 to create an automatic-only splitter situation, as valve 134 moves to its second position, wherein the pilot conduit 108 controlled by manual selector valve 104 is blocked at inlet 138, and thus, the series connection through port 140 to the pilot valve 112 is blocked. With valve 134 in the second or actuated position thereof, the manual selector 104 is ineffective to control pilot valve 112 or splitter actuator 86.

In the current example, ninth and tenth speeds are the AUTO mode gear ratios, while eighth speed is the "entry gear ratio". A shift or intent to shift into the AUTO mode is confirmed when either:

(1) gear ratio is the entry gear ratio, and
 (2) vehicle speed exceeds a first reference value (REF₁), followed by
 (3) a shift into neutral;

OR

(1) vehicle speed exceeds the first reference value, and
 (2) gear ratio is one of the AUTO mode ratios.

The first reference value (REF₁) is an output shaft speed at which a manual upshift from the entry gear is expected to occur, usually about the minimum output shaft speed at which an upshift from the entry gear is expected to occur.

When in the AUTO mode of operation, manual control 104 is bypassed and, based upon vehicle speed as indicated by the output shaft speed OS and/or the other sensed parameters, the control 124 will automatically determine if an automatic upshift from ninth to tenth or an automatic downshift from tenth to ninth is required, and will control engine fueling and the second solenoid-controlled valve 136 to implement same. With valve 134 actuated and valve 136 in its normal or default position, pilot conduit 110 is exhausted at port 144 of valve 134, and pilot valve 112 will exhaust the control chamber 114 of the piston/cylinder assembly 86, causing the piston to urge the splitter clutch in the low splitter ratio direction. With the second solenoid-controlled valve 136 actuated, pilot conduit 110 is connected to source pressure through inlet 146 and outlet 148 of valve 136, regardless of the position of valve 134, and pilot valve 112 will cause

control chamber 114 to be pressurized, causing the piston 118 to urge the splitter clutch in the high splitter ratio direction. Valve 134 may be deactivated whenever valve 136 is energized to reduce heat generation.

In addition to causing the splitter clutch to be properly positioned in the AUTO mode, controller 124 will also cause the engine to be properly fueled to disengage the existing splitter ratio and synchronized for engaging the target splitter ratio. Upon sensing an eighth-to-ninth upshift into AUTO mode, the engine will be caused to synchronize for the required main and splitter clutch engagement.

In the current example, continuing operation in the AUTO mode is confirmed when either:

- (1) the confirmed gear ratio is an AUTO mode ratio (*i.e.*, ninth or tenth), and
- (2) vehicle speed exceeds the first reference value ($OS \cdot GR_{ENTRY} \geq$ the expected manual upshift RPM from the entry gear);

OR

an AUTO mode shift (ninth-tenth, tenth-ninth) is in progress.

Upon sensing that a shift from AUTO mode has occurred, the controller 124 will cause solenoid driver 132 to deactivate both solenoids to return splitter control to the operator. In the current example, a non-AUTO mode condition is confirmed when either:

- (1) an AUTO mode shift is not in progress, and
- (2) vehicle speed is less than a second reference value (REF_2), followed by
- (3) a shift into neutral;

OR

- (1) an AUTO shift is in progress, and
- (2) after a given period of time, engagement in an AUTO mode ratio cannot be confirmed;

OR

engagement in a non-AUTO mode ratio is confirmed.

The first, immediately preceding example involves a downshift out of AUTO mode, while the second example involves an apparent operator shift to main section neutral during an AUTO mode shift event.

In causing synchronous conditions for engagement of a target gear ratio, the engine is commanded to assume a rotational speed equal to true synchronous speed ($ES = OS \cdot GR_T$) plus or minus an offset value X equal to about 30 to 50 RPM. Accordingly, the engine is alternately commanded to a speed ($ES = (OS + X) \cdot GR_T$), and then a speed ($ES = (OS - X) \cdot GR_T$).

To confirm engagement/non-engagement, the value of ES/OS is compared over a period of time to known gear ratios plus or minus a given percent Y (such as 0.5

to 1.5%). Thus, by way of example, over a period of time, if $ES/OS = GR^*(1 \pm Y\%)$, then confirmation of engagement of GR is true. The offset X and the percentage error Y are selected so that at $ES = (OS + X) \cdot GR_T$, or at $ES = (OS - X) \cdot GR_T$, ES/OS will not equal $GR^*(1 \pm Y\%)$.

The foregoing, as discussed in aforementioned pending U.S. Patent Application Serial No. 08/649,829, allows the use of speed signals to confirm engaged and neutral conditions without false readings due to engine synchronizing.

To confirm disengagement (of the entry gear ratio or of one of the AUTO mode ratios), the quotient of ES/OS is compared to the numerical value of the disengaging gear, plus or minus a disengaging gear error value, which may exceed the magnitude of the gear error value used to confirm engagement. For example, the disengaging gear error value may equal 1.5%, while the engaging gear error value may equal 1%.

Additionally, the gear error value used for confirming disengagement may be set larger on the positive side of synchronous of the disengaging gear than on the negative side to minimize false indications of neutral. Speed separations while still in gear tend to be higher on the positive side of synchronous due to the higher driving torque (the engine driving the vehicle tends to produce a greater positive torque magnitude than the negative torque produced when coasting with the vehicle driving the engine). Providing a larger $Pos_Disengage_Gear_Error$ and a smaller $Neg_Disengage_Gear_Error$ allows for protection against false indications of neutral on the positive side caused by aggressive throttle application, while still providing for a quick confirmation of neutral in the negative direction (the direction in which neutral is confirmed on most shifts).

In the preferred embodiment, the calculated gear ratio, ES/OS , is compared to an expanding window of error values and will be confirmed as disengaged only if it continues to remain outside the window. In the current example (see Figure 6), the calculated gear ratio must fall outside a range from:

[Engaged $GR^*(1 + (40 \cdot Counter \cdot Loop_Time \cdot Neg_Disengage_Gear_Error))$]
to

[Engaged $GR^*(1 + (40 \cdot Counter \cdot Loop_Time \cdot Pos_Disengage_Gear_Error))$],
where Counter is incremented by one each time this is true and decremented each time this is not true (minimizing at a value of 1). Disengagement is confirmed when the Counter reaches or exceeds a value equal to ($Synch_Disengage_Time/Loop_Time$). In the preferred embodiment, the values of $Neg_Disengage_Gear_Error = 1\%$, $Pos_Disengage_Gear_Error = 1.5\%$, and the maximum value of ($40 \cdot Counter \cdot Loop_Time$) = 6.

The advantage of this "expanding window" over a fixed error band (prior art) is that it allows disengagement confirmation to start sooner (using the relatively

small initial error window) while simultaneously providing better protection against false confirmations of neutral (using the relatively large, fully expanded window before confirming). If the calculated gear ratios fall back within the window during the disengagement confirmation process, the window will decrement to the next smaller value (or to the smallest window) and upon the calculated gear ratio falling outside the window, the disengagement process will continue. The advantage gained with this "contracting window" over immediately resetting to the smallest error window is that it maintains a quick confirmation of true disengagement even if one data point falls inside the expanding error bounds, while preventing false neutral confirmation with transient speed separations induced by large torque oscillations.

Upon an electrical power failure, the solenoid-controlled valves will return to the open positions thereof, fluidly connecting conduits 108 and 110, and allowing manual selection of all ten forward ratios. Upon the solenoid driver detecting conditions indicative of a failure at one or both solenoids, the controller will cause both solenoids to be de-energized again, causing the two valves 134 and 136 to assume the open positions thereof, and allow manual selection of all ten forward ratios.

The control valve assembly 94, thus, provides a control allowing both manual and automatic splitter shifting, provides a favorable failure mode and as a module requires only four additional fluid connections (conduit 108 to port 138, conduit 110 to port 148, source S to port 146 and exhaust E_X to port 144) to the normally utilized manual splitter control.

As used herein, "main section" ratio positions will include the 1/2, 2/3, 3/4, 5/6, 7/8 and 9/10(A) ratio positions, and the range section is considered a portion of the manually shifted main section.

In the event of a failure in operating solenoids, in the splitter actuators, in the devices providing signals (ES, OS) indicative of engine and/or output shaft rotational speeds or the like, the preferred degraded mode is operation as a totally manual 10-speed splitter-type transmission, as illustrated in Figures 1 and 2.

When in the AUTO mode, upon sensing an actuator or a solenoid speed sensor fault or the like, the transmission is retained in its currently engaged splitter ratio until main section neutral can be confirmed, and then the splitter valve assembly 94 is returned to manual control. The control principle is not to go from an engaged splitter ratio to possible splitter neutral until the system is sure the operator has manually shifted into neutral. This will assure no unintended neutral conditions, although the system may drive as a wide-step 5-speed (*i.e.*, only 1-3-5-7-9 or 2-4-6-8-10 available) until neutral can be confirmed.

Accordingly, it may be seen that an improved compound transmission and shift control unit has been provided.

Although the present invention has been described with a certain degree of particularity, it is understood that

the description of the preferred embodiment is by way of example only and that numerous changes to form and detail are possible without departing from the spirit and scope of the invention as hereinafter claimed.

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Claims

1. A method for controlling an automated mechanical transmission system comprising a splitter-type mechanical transmission having an input shaft driven by a fuel-controlled engine, an output shaft, a manually shifted main section and a splitter section having a splitter section actuator, said splitter section actuator responsive in a manually shifted mode to manually supplied command signals and in an automatic mode of operation, to controller-supplied command signals to control shifting of said splitter section, said method comprising:

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sensing values of input signals, including signals indicative of input and output shaft rotational speeds, to determine the existence of system faults;

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upon sensing a system fault when in the automatic mode of operation, maintaining existing splitter section actuator condition until a main section neutral condition is sensed and, upon sensing a main section neutral condition, causing said splitter actuator to be controlled only by said manually supplied command signals.

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2. The method of claim 1 wherein said system operates in said automatic mode of operation only in certain main section ratios.

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3. The method of claim 1 wherein said splitter section actuator comprises at least one solenoid-controlled valve responsive to said manually supplied control signals.

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4. A machine for controlling an automated mechanical transmission system comprising a splitter-type mechanical transmission having an input shaft driven by a fuel-controlled engine, an output shaft, a manually shifted main section and a splitter section having a splitter section actuator, said splitter section actuator responsive in a manually shifted mode to manually supplied command signals and in an automatic mode of operation, to controller-supplied command signals to control shifting of said splitter section, said machine comprising:

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logic elements effective to sense values of input signals, including signals indicative of input and output shaft rotational speeds, to determine the existence of system faults; and logic elements effective, upon sensing a sys-

tem fault when in the automatic mode of operation, to maintain existing splitter section actuator condition until a main section neutral condition is sensed and, upon sensing a main section neutral condition, causing said splitter actuator to be controlled only by said manually supplied command signals.

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5. The machine of claim 4 wherein said system operates in said automatic mode of operation only in certain main section ratios. 10
6. The machine of claim 4 wherein said splitter section actuator comprises at least one solenoid-controlled valve responsive to said manually supplied control signals. 15

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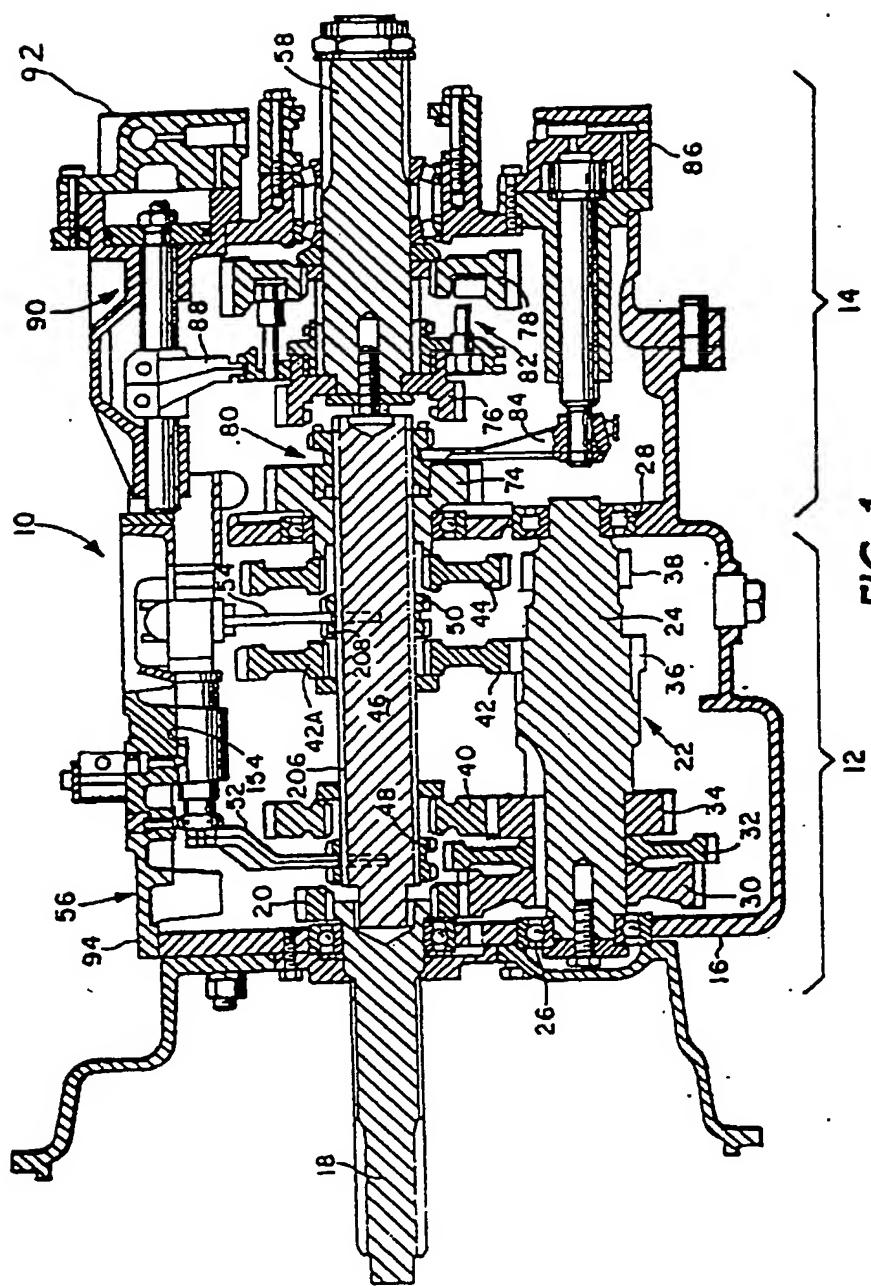


FIG. 1
PRIOR ART

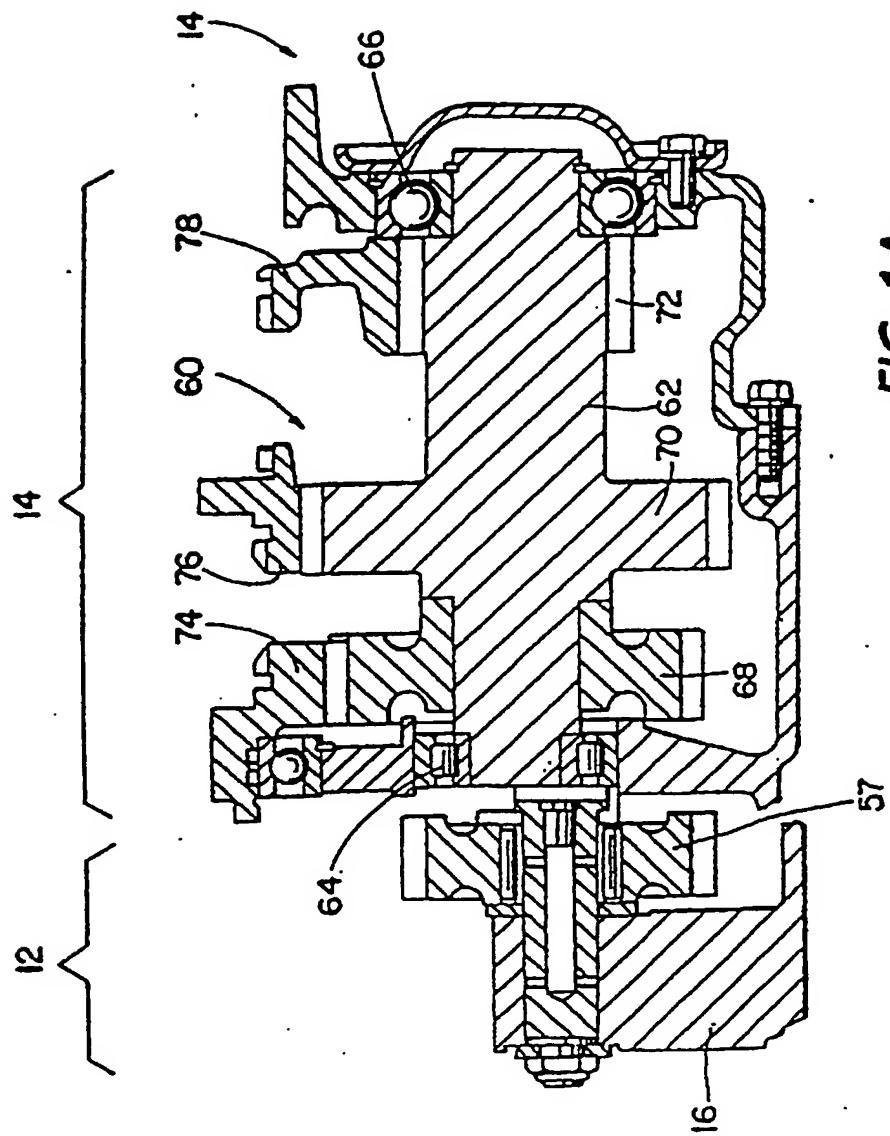


FIG. 1A
PRIOR ART

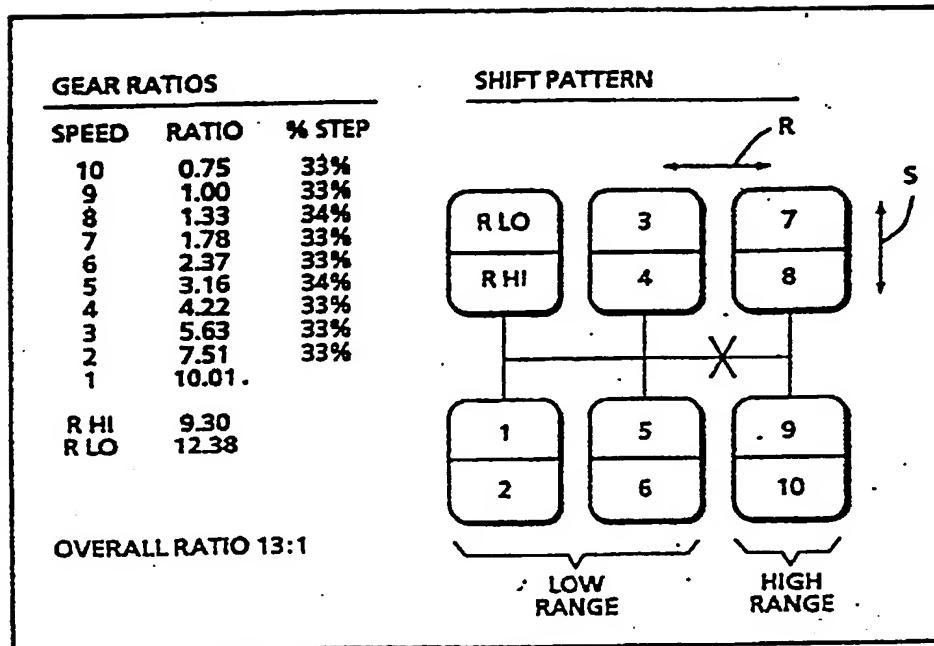
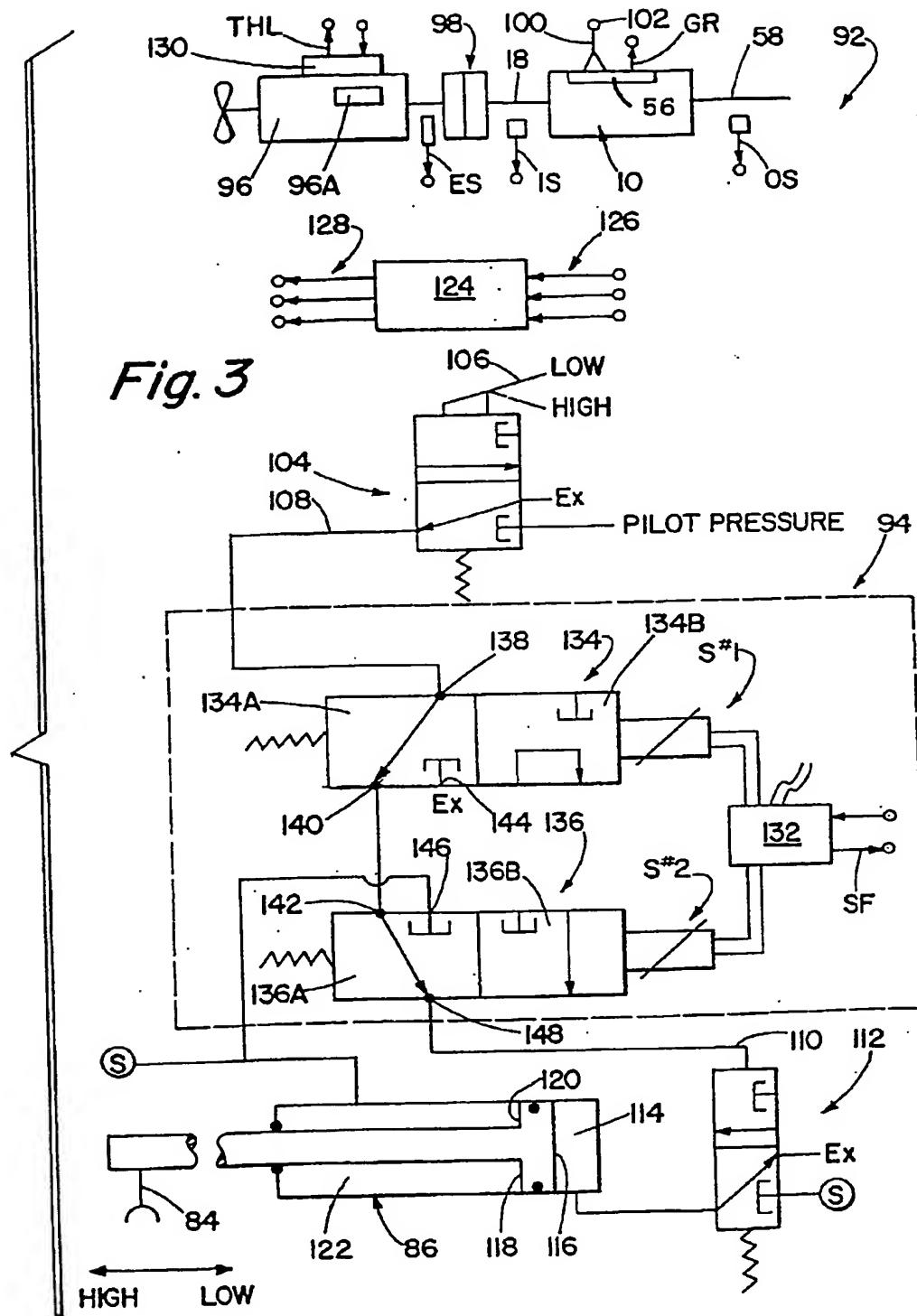


FIG. 2
PRIOR ART



VALVE TABLE

GEAR	S# 1	S# 2
1-8	OFF	OFF
9	ON	OFF
10	OFF/ON	ON

FIG 4.

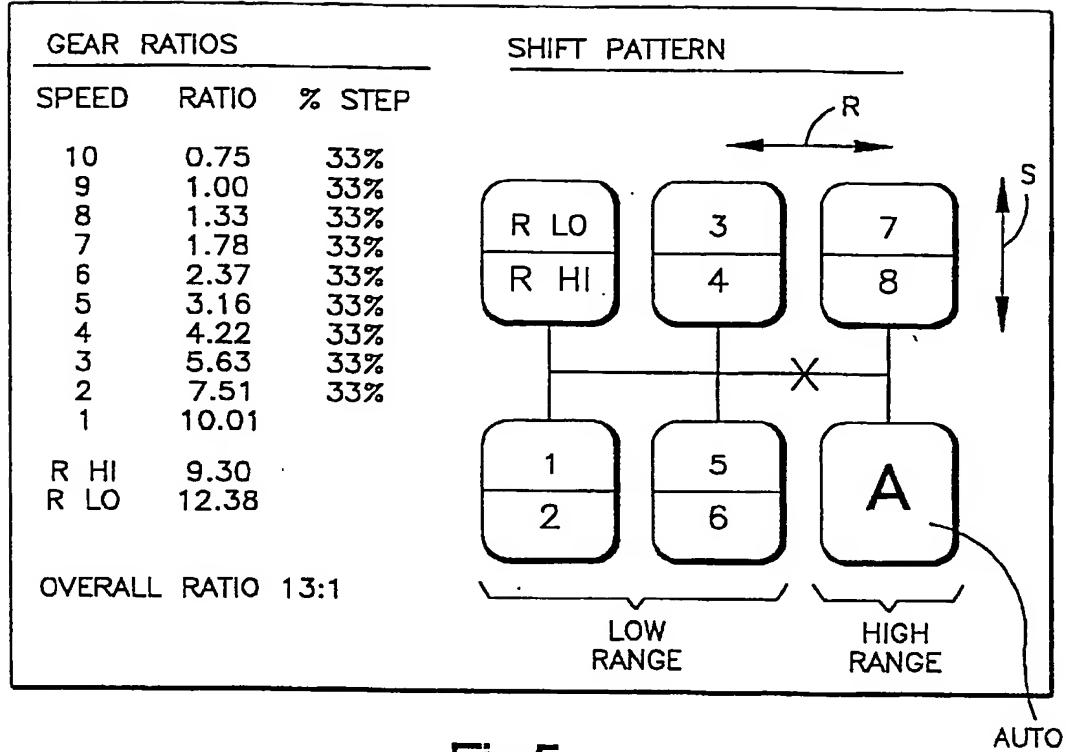


Fig.5

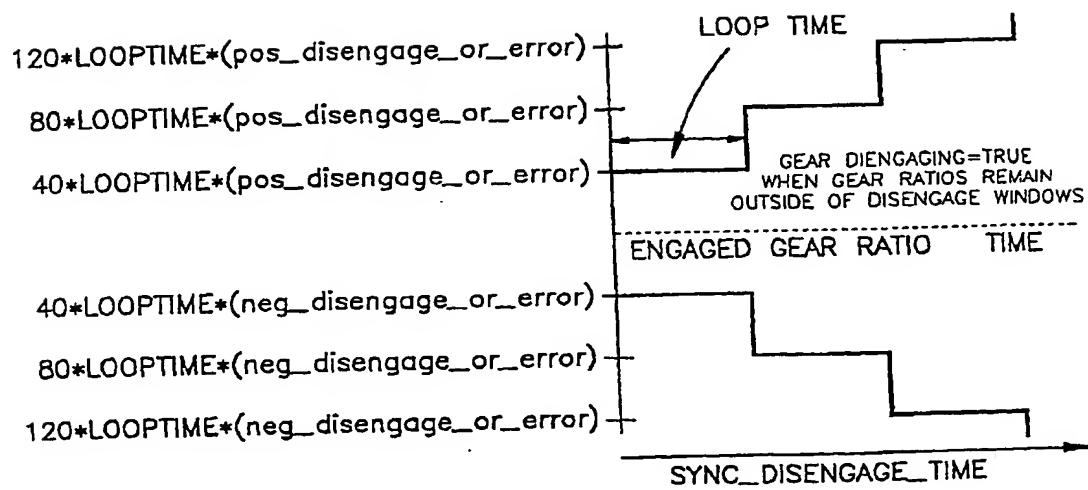


Fig.6

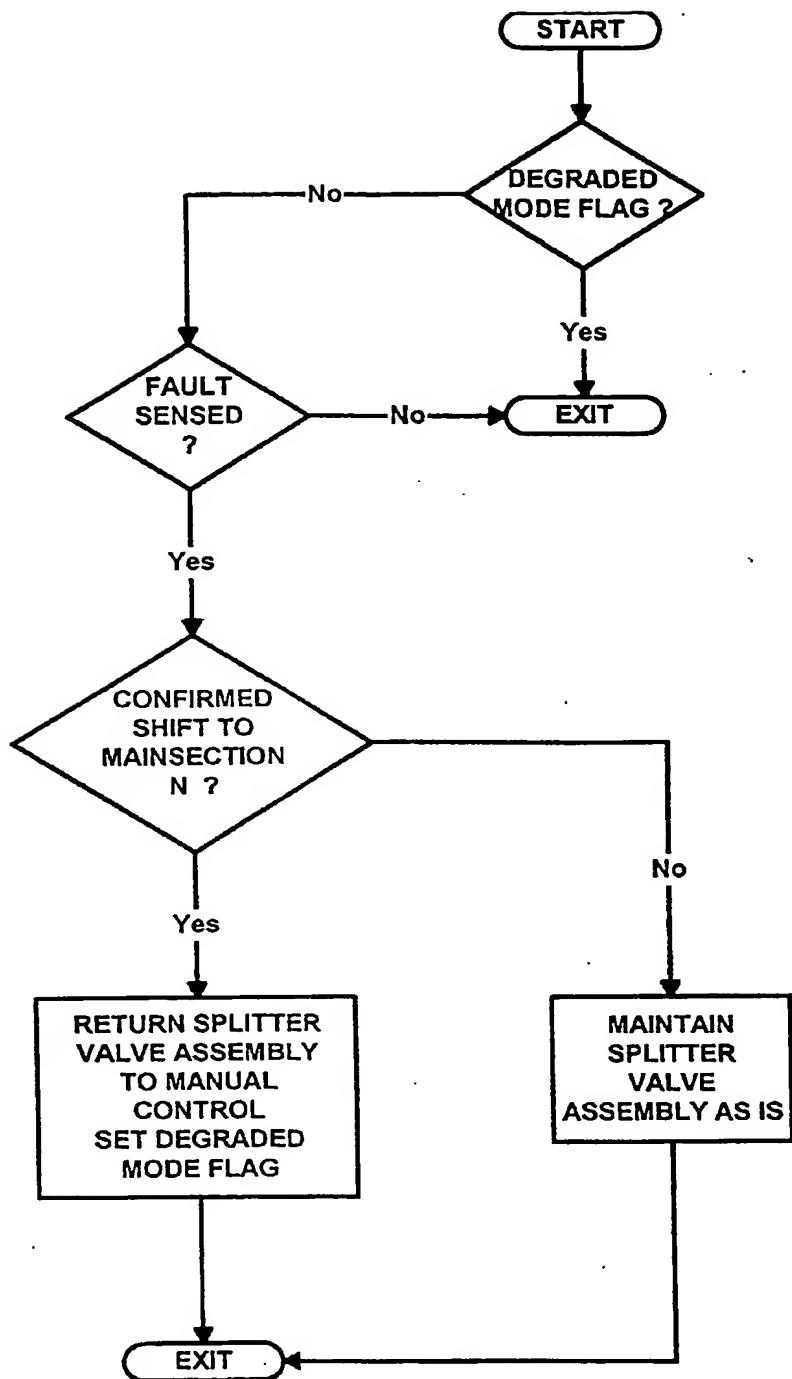


FIG. 7

(19)



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(30) Priority: 05.02.1997 US 790209

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(54) Operation mode transition of an automated transmission

(57) A degraded mode of operation (Figure 7) for a partially automated mechanical transmission system having a splitter-type mechanical transmission with a splitter section automatically shifted in only certain ratios (ninth/tenth). Upon sensing certain system faults when in this automatic splitter shifting mode, the splitter section is retained, as is, until main section neutral can be confirmed, at which time the splitter section is returned to manual control for all transmission ratios.

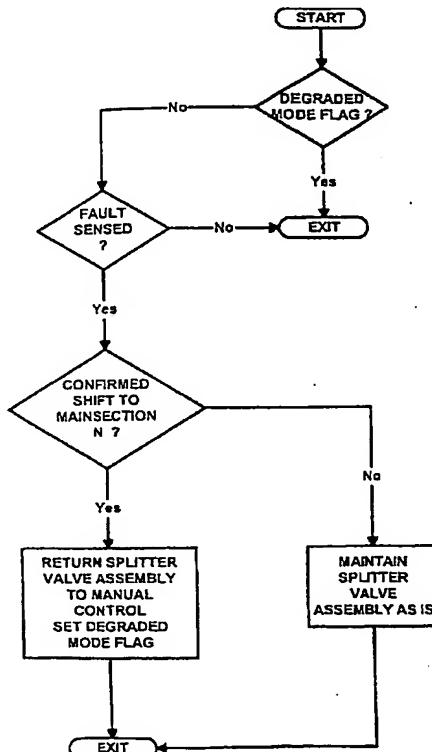


FIG. 7



European Patent
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EUROPEAN SEARCH REPORT

Application Number
EP 98 30 0833

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			F16H B60K
<p>The present search report has been drawn up for all claims</p>			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	22 February 1999	Daehnhardt, A	
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date O : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
X : particularly relevant if taken alone Y : particularly relevant if combined with another/ document of the same category A : technological background O : non-written disclosure P : intermediate document			

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(54) Operation mode transition of an automated transmission

Verfahren zum Wechseln des Betriebsmodus eines automatisierten Getriebes

Méthode de commande pour le passage du mode de fonctionnement d'une transmission auxiliaire

(84) Designated Contracting States:
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Kalamazoo, MI 49001-4323 (US)

(30) Priority: 05.02.1997 US 790209

(74) Representative: Clarke, Geoffrey Howard et al
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P.O.Box 75777
1118 ZX Luchthaven Schiphol (NL)

(43) Date of publication of application:
12.08.1998 Bulletin 1998/33

(73) Proprietor: EATON CORPORATION
Cleveland, Ohio 44114-2584 (US)

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EP-A- 0 110 428 EP-A- 0 547 829
EP-A- 0 552 557 EP-A- 0 552 867
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(72) Inventors:

• Steeby, Jon A.
Schoolcraft, MI 49087-9780 (US)

EP 0 857 897 B1

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Description**BACKGROUND OF THE INVENTION****RELATED APPLICATIONS**

[0001] This application is related to the following co-pending U.S. applications, all assigned to EATON CORPORATION, the assignee of this application:

Serial No. 08/649,829 [▲] = EP-A-805 062

Filed: 30/04/96

Title: SYNCHRONIZING AND GEAR ENGAGEMENT SENSING LOGIC FOR AUTOMATED MECHANICAL TRANSMISSION SYSTEMS

Serial No. 795,918 [96-TRN-113] [▲] = EP-A-857 899

Filed: 05/02/97

Title: AUTOMATED TRANSMISSION SYSTEM POWER-DOWN

Serial No. 796,001 [96-TRN-114] [▲] = EP-A-857 894

Filed: 05/02/97

Title: SENSING MANUAL SHIFT INTO AUTOMATED UPPER RATIOS

Serial No. 796,006 [96-TRN-116] [▲] = EP-A-857 604

Filed: 05/02/97

Title: AUTOMODE-TO-NEUTRAL LOGIC

Serial No. 795,616 [96-TRN-117] [▲] = EP-A-857 898

Filed: 05/02/97

Title: ANTI-HUNT LOGIC

Serial No. 795,615 [96-TRN-119] [▲] = EP-A-857 895

Filed: 05/02/97

Title: DISENGAGEMENT CONFIRMATION

Serial No. 790,210 [96-TRN-121] [▲] = EP-A-857 896

Filed: 05/02/97

Title: ENGAGEMENT OF GEAR RATIO CONFIRMATION

FIELD OF THE INVENTION

[0002] The present invention relates to a fault-tolerant logic for a partially automated mechanical transmission system having automated splitter shifting in at least one main section ratio position. The features of the preamble of claim 1 and 4, respectively, are known from EP-A-742 393.

DESCRIPTION OF THE PRIOR ART

[0003] Partially automated vehicular transmission systems requiring manual shifting in the lower ratios and having a control for automated shifting in the upper ra-

tios are known in the prior art, as may be seen by reference to U.S. Patents No. 4,722,248; 4,850,236; 5,038,627; 5,393,276; 5,393,277 and 5,498,195.

[0004] Splitter and combined range and splitter-type compound vehicular transmissions requiring manual splitter shifting are well known in the prior art, as may be seen by reference to U.S. Patents No. 3,799,002; 4,754,665; 4,974,468; 5,000,060; 5,370,013 and 5,390,561. Transmissions with automatic splitter shifting are known in the prior art, as may be seen by reference to U.S. Patent No. 5,435,212.

[0005] Fault-tolerant and limp-home routines for automated mechanical transmission systems are known in the prior art, as may be seen by reference to U.S. Patents No. 5,109,721 and 5,157,607.

SUMMARY OF THE INVENTION

[0006] In accordance with the present invention, a new and improved control system/method for an automated mechanical transmission system having automated splitter shift in certain ratios only and manual splitter shifting in other ratios and an improved fault-tolerant degraded mode of operation is provided.

[0007] The foregoing is accomplished by providing a logic which, in the event of faults which will adversely affect automatic splitter shifting, maintains the automated splitter shifting mechanism engaged in the currently engaged splitter ratio until a manual shift into neutral is sensed, at which time the splitter mechanism is returned to manual control.

[0008] Accordingly, it is an object of the present invention to provide a new and improved fault-tolerant degraded mode of operation for a partially automated mechanical transmission system having manually and automatically controlled splitter shifting.

[0009] This and other objects and advantages of the present invention will become apparent from a reading of the following description of the preferred embodiment taken in connection with the attached drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0010] Figures 1 and 1A are sectional views of a typical splitter or combined splitter and range-type compound transmission.

[0011] Figure 2 is a schematic illustration of the manual shift pattern and ratio steps for the transmission of Figures 1 and 1A.

[0012] Figure 3 is a schematic illustration of a partially automated vehicular mechanical transmission system having both manual and automatic splitter shifting and utilizing the control of the present invention.

[0013] Figure 4 is a valve table for the control valve assembly utilized in the system of Figure 3.

[0014] Figure 5 is a schematic illustration, similar to Figure 2, of the shift pattern and ratio steps for the transmission system of Figure 3.

[0015] Figure 6 is a graphical representation of the disengagement confirmation logic of the system of Figure 3.

[0016] Figure 7 is a schematic illustration, in flow chart format, of the fault-tolerant degraded mode of operation logic of the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT

[0017] Figures 1, 1A and 2 illustrate a typical combined splitter and range-type compound mechanical transmission 10 of the type advantageously utilized in connection with the control of the present invention.

[0018] Transmission 10 comprises a main transmission section 12 connected in series with an auxiliary transmission section 14 having both range and splitter-type gearing. Typically, transmission 10 is housed within a single multi-piece housing 16 and includes an input shaft 18 driven by a prime mover (such as a diesel engine) through a selectively disengaged, normally engaged friction master clutch.

[0019] In the main transmission section 12, the input shaft 18 carries an input gear 20 for driving at least one countershaft assembly 22. Preferably, as is well known in the prior art and as is illustrated in U.S. Patents No. 3,105,395 and 3,335,616, input gear 20 simultaneously drives a plurality of substantially identical main section countershaft assemblies at substantially identical rotational speeds. Each of the main section countershaft assemblies comprises a main section countershaft 24 supported by bearings 26 and 28 in housing 16 and is provided with main section countershaft gears 30, 32, 34, 36 and 38 fixed thereto. A plurality of main section drive or main shaft gears 40, 42 and 44 surround the transmission main shaft 46 and are selectively clutchable, one at a time, to the main shaft 46 for rotation therewith by sliding clutch collars 48 and 50, as is well known in the art. Clutch collar 48 may also be utilized to clutch input gear 20 to the main shaft 46 to provide a direct drive relationship between the input shaft 18 and the main shaft 46. Preferably, each of the main section main shaft gears encircles the main shaft 46 and is in continuous meshing engagement with and is floatingly supported by the associated countershaft gear groups, which mounting means and special advantages resulting therefrom are explained in greater detail in aforementioned U.S. Patents No. 3,105,395 and 3,335,616. Typically, clutch collars 48 and 50 are axially positioned by means of shift forks or yokes 52 and 54, respectively, associated with a shift bar housing assembly 56 of the type illustrated in U.S. Patents No. 4,920,815 and 5,000,060. Clutch collars 48 and 50 are, in the preferred embodiment, of the well-known, non-synchronized, double-acting jaw clutch type.

[0020] Main section main shaft gear 44 is the reverse gear and is in continuous meshing engagement with countershaft gears 38 by means of conventional intermediate idler gears 57 (see Figure 1A). Main section

countershaft gear 32 is provided for powering power takeoff devices and the like. Jaw clutches 48 and 50 are 3-position clutches in that they may be positioned in a centered axially non-displaced, non-engaged position as illustrated or in a fully rightwardly engaged or fully leftwardly engaged position.

[0021] Auxiliary transmission section 14 is connected in series with main transmission section 12 and is of the 3-layer, 4-speed combined splitter/range type, as illustrated in above-mentioned U.S. Patent No. 4,754,665. Main shaft 46 extends into the auxiliary section 14 and is journaled in the inward end of the output shaft 58 which extends from the rearward end of the transmission.

[0022] Auxiliary transmission section 14 includes, in the preferred embodiment thereof, a plurality of substantially identical auxiliary countershaft assemblies 60 (see Figure 1A), each comprising an auxiliary countershaft 62 supported by bearings 64 and 66 in housing 16 and carrying three auxiliary section countershaft gears 68, 70 and 72 fixed for rotation therewith. Auxiliary countershaft gears 68 are constantly meshed with and support auxiliary section splitter gear 74. Auxiliary countershaft gears 70 are constantly meshed with and support auxiliary section splitter/range gear 76 which surrounds the output shaft 58 at the end thereof adjacent the coaxial inner end of main shaft 46. Auxiliary section countershaft gears 72 constantly mesh with and support auxiliary section range gear 78, which surrounds the output shaft 58. Accordingly, auxiliary section countershaft gears 68 and splitter gear 74 define a first gear layer, auxiliary section countershaft gears 70 and splitter/range gear 76 define a second gear layer and auxiliary section countershaft gears 72 and range gear 78 define a third layer, or gear group, of the combined splitter and range-type auxiliary transmission section 14.

[0023] A sliding 2-position jaw clutch collar 80 is utilized to selectively couple either the splitter gear 74 or the splitter/range gear 76 to the main shaft 46, while a 2-position synchronized clutch assembly 82 is utilized to selectively couple the splitter/range gear 76 or the range gear 78 to the output shaft 58.

[0024] The splitter jaw clutch 80 is a 2-position clutch assembly which may be selectively positioned in the rightwardmost or leftwardmost positions for engaging either gear 76 or gear 74, respectively, to the main shaft 46. Splitter jaw clutch 80 is axially positioned by means of a shift fork 84 controlled by a 2-position piston actuator 86 or splitter section actuator as referred to in the claims, which normally is operable by a driver selection switch such as a button or the like on the shift knob, as is known in the prior art. Two-position synchronized range clutch assembly 82 is also a 2-position clutch which may be selectively positioned in either the rightwardmost or leftwardmost positions thereof for selectively clutching either gear 78 or 76, respectively, to output shaft 58. Clutch assembly 82 is positioned by means of a shift fork 88 operated by means of a 2-position pis-

ton device 90, the actuation and control of which is described in greater detail in aforementioned U.S. Patent No. 4,974,468.

[0025] As may be seen by reference to Figures 1-2, by selectively axially positioning both the splitter clutch 80 and the range clutch 82 in the forward and rearward axial positions thereof, four distinct ratios of main shaft rotation to output shaft rotation may be provided. Accordingly, auxiliary transmission section 14 is a 3-layer auxiliary section of the combined range and splitter type providing four selectable speeds or drive ratios between the input (main shaft 46) and output (output shaft 58) thereof. The main section 12 provides a reverse and three potentially selectable forward speeds. However, one of the selectable main section forward gear ratios, the low speed gear ratios associated with main shaft gear 42, is not utilized in the high range. Thus, transmission 10 is properly designated as a "(2+1)x(2x2)" type transmission providing nine or ten selectable forward speeds, depending upon the desirability and practicality of splitting the low gear ratio.

[0026] While clutch 82 (the range clutch) should be a synchronized clutch, double-acting clutch collar 80 (the splitter clutch) is not required to be synchronized. The shift pattern for manually shifting transmission 10 is schematically illustrated in Figure 2. Divisions in the vertical direction at each gear lever position signify splitter shifts, while movement in the horizontal direction from the 3/4 and 5/6 leg of the H pattern to the 7/8 and 9/10 leg of the H pattern signifies a shift from the low range to the high range of the transmission. As discussed above, manual splitter shifting is accomplished in the usual manner by means of a vehicle operator-actuated splitter button or the like, usually a button located at the shift lever knob, while operation of the range clutch shifting assembly is an automatic response to movement of the gear shift lever between the central and rightward-most legs of the shift pattern, as illustrated in Figure 2. Range shift devices of this general type are known in the prior art and may be seen by reference to U.S. Patents No. 3,429,202; 4,455,883; 4,561,325 and 4,663,725. Manually operated splitter and range shift actuators are known in the prior art and may be seen by reference to U.S. Patents No. 5,193,410; 5,199,314 and 5,329,826.

[0027] A partially automated vehicular mechanical transmission system 92 utilizing the control system of the present invention is illustrated in Figure 3. Partially automated system 92 is of the type requiring manual shifting in the lower gear ratios (first through eighth) and, after initial manual selection of one of the upper two ratios, providing automatic shifting in the upper gear ratios (ninth and tenth), as described in aforementioned U.S. Patents No. 4,722,248; 4,850,236; 5,038,027 and 5,393,276. The shift pattern for partially automated operation of the system 92 is schematically illustrated in Figure 5.

[0028] The system includes a splitter control valve as-

sembly 94 and a prime mover (such as diesel engine 96) driving the input shaft 18 of transmission 10 through a master friction clutch 98. The transmission 10 includes a shift lever 100 having a shift knob 102, which is associated with the shift bar housing 56 for manually shifting main section 12 and the range clutch 82 of auxiliary section 14.

[0029] A manually operated splitter valve 104, having a selector lever or button 106, is provided, usually on or integral with the shift knob, for manually shifting the splitter clutch 80. Splitter valve 104 is a 2-position, 3-way manually operated valve effective to selectively connect a first pilot conduit 108 to exhaust ("Ex") or to pilot pressure, respectively, to manually select either the high or low splitter ratio. The pilot pressure may be equal to supply pressure ("S") or to a lower value. In a typical on-board pneumatic system, supply is filtered, regulated air at about 60 to 80 psi (approx. 4.5 bar).

[0030] The first pilot conduit 108 may fluidly communicate with a second pilot conduit 110 in series through the control valve assembly 94 of the present invention. The second pilot conduit 110 is effective to act on a 2-position, 3-way pilot valve 112, which is effective to normally vent or selectively pressurize a control chamber 114 of the splitter piston/cylinder actuator assembly 86. Chamber 114 is exposed to the larger area face 116 of a differential area piston 118 having a smaller area face 120 constantly exposed to supply pressure in biasing chamber 122. As is known, a spring may be utilized in place of or in combination with smaller area piston face 120 to bias piston 118 rightwardly, as seen in Figure 3.

[0031] As may be seen, when pilot conduit 110 is exhausted, pilot valve 112 will connect control chamber 114 to exhaust, and supply pressure acting on smaller area face 120 will cause shift fork 84 to move splitter clutch 80 to engage gear 76 for the low splitter ratio, and when pilot conduit 110 is pressurized, valve 112 will move against a bias to a position for pressurizing control chamber 114, causing the piston 118 to move leftwardly to cause splitter clutch 80 to engage gear 74 for the high splitter ratio.

[0032] Except for interposing the control valve assembly 94 in series between pilot conduits 108 and 110, the above-described components are structurally and functionally equivalent to components utilized to shift the manually shifted transmission of Figures 1, 1A and 2.

[0033] To provide the partially automated operation of system 92, a controller 124, preferably a microprocessor-based controller, is provided for receiving input signals 126 and for processing same according to predetermined logic rules to issue command output signals 128 to various system actuators, such as an engine fuel control 130 and a solenoid driver and fault detection unit 132. Controllers of this type may be seen by reference to U.S. Patents No. 4,361,060 and 4,595,986. The program for controller 124 is stored on a computer-readable medium such as a floppy disk, hard drive, CD-rom, tape or other external or internal storage medium.

[0034] Sensors for sensing engine speed (ES) and/or input shaft speed (IS) and output shaft speed (OS) may be provided, as well as sensors for sensing engine fueling THL and solenoid faults SF, all of which provide input signals indicative thereof to the controller 124. With the clutch 98 engaged, input shaft speed may be assumed to equal engine speed.

[0035] As is known, the engine 96 may have a built-in controller 96A and/or may communicate with controller 124 by an electronic data link of the type conforming to SAE J-1922, SAE J-1939, ISO 11898 or the like. All or a portion of controller 124 may be defined by hardware and/or software associated with engine controller 96A. A sensor may be provided for providing a signal (GR) indicative of engaged gear ratio or gear ratio may be calculated and confirmed by dividing input shaft speed or engine speed by output shaft speed ($GR = ((IS - ES)/OS \mp \text{error?})$).

[0036] The control valve assembly 94 of the present invention is interposed in series between the standard manual splitter shift selection valve 104 and the standard pilot valve 112/splitter actuator 86 and is operated in response to command output signals from controller 124. The assembly includes, in series, a first 2-position, 3-way solenoid-controlled valve 134 and a second 2-position, 3-way solenoid-controlled valve 136 and a solenoid driver and fault detection unit 132 operating in response to command output signals from the controller.

[0037] Valve 134 has an inlet 138 connected to pilot conduit 108 and two outlets 140 (connected to one inlet 142 of valve 136) and 144 (connected to exhaust). Valve 134 has a first normal or default position wherein inlet 138 is connected to outlet 140, and thus, to inlet 142 of valve 136, while outlet 144 of valve 134 is blocked. Valve 134 has a second or actuated position upon energizing the first solenoid S#1 wherein outlet 140 is connected to exhaust at outlet 144 and inlet 138 is blocked.

[0038] Valve 136 has two inlets 142 (connected to the outlet 140 of valve 134) and 146 (connected to the source of pressurized fluid) and an outlet 148 connected to the second pilot conduit 110 controlling the pilot valve 112. Valve 136 has a first normal or default position wherein inlet 142 is connected to outlet 148 and the inlet 146 from source pressure is blocked, and a second actuated position upon energizing the second solenoid S#2 wherein inlet 142 is blocked and source pressure at inlet 146 communicates with outlet 148 and pilot conduit 110.

[0039] The valve table for operation of the solenoid-operated valves is set forth in Figure 4.

[0040] The controller 124 senses a manual splitter operation mode by sensing a shift bar condition GR other than AUTO (see Figure 5). In this mode (i.e., gear ratios 1-8), the solenoid driver is commanded to deenergize both of the solenoids, and the valves 134 and 136 will assume the default positions thereof. Pilot conduit 108 will communicate with pilot conduit 110 through the valves 134 and 136, and the actuator 86 will be under

the manual control of selector valve 104.

[0041] AUTO or not-AUTO mode conditions may be sensed by position sensors or by processing the ES and OS signals according to predetermined logic rules.

5 [0042] Upon sensing a manual shift to the AUTO position, the controller will cause the solenoid driver 132 to energize the first solenoid S#1 to create an automatic-only splitter situation, as valve 134 moves to its second position, wherein the pilot conduit 108 controlled by manual selector valve 104 is blocked at inlet 138, and thus, the series connection through port 140 to the pilot valve 112 is blocked. With valve 134 in the second or actuated position thereof, the manual selector 104 is ineffective to control pilot valve 112 or splitter actuator 86.

10 [0043] In the current example, ninth and tenth speeds are the AUTO mode gear ratios, while eighth speed is the "entry gear ratio". A shift or intent to shift into the AUTO mode is confirmed when either:

15 20 (1) gear ratio is the entry gear ratio, and
(2) vehicle speed exceeds a first reference value (REF₁), followed by
(3) a shift into neutral;

25 OR

30 (1) vehicle speed exceeds the first reference value, and
(2) gear ratio is one of the AUTO mode ratios.

35 [0044] The first reference value (REF₁) is an output shaft speed at which a manual upshift from the entry gear is expected to occur, usually about the minimum output shaft speed at which an upshift from the entry gear is expected to occur.

40 [0045] When in the AUTO mode of operation, manual control 104 is bypassed and, based upon vehicle speed as indicated by the output shaft speed OS and/or the other sensed parameters, the control 124 will automatically determine if an automatic upshift from ninth to tenth or an automatic downshift from tenth to ninth is required, and will control engine fueling and the second solenoid-controlled valve 136 to implement same. With valve 134 actuated and valve 136 in its normal or default

45 position, pilot conduit 110 is exhausted at port 144 of valve 134, and pilot valve 112 will exhaust the control chamber 114 of the piston/cylinder assembly 86, causing the piston to urge the splitter clutch in the low splitter ratio direction. With the second solenoid-controlled valve 136 actuated, pilot conduit 110 is connected to source pressure through inlet 146 and outlet 148 of valve 136, regardless of the position of valve 134, and pilot valve 112 will cause control chamber 114 to be pressurized, causing the piston 118 to urge the splitter clutch in the high splitter ratio direction. Valve 134 may be deactivated whenever valve 136 is energized to reduce heat generation.

50 [0046] In addition to causing the splitter clutch to be

properly positioned in the AUTO mode, controller 124 will also cause the engine to be properly fueled to disengage the existing splitter ratio and synchronized for engaging the target splitter ratio. Upon sensing an eighth-to-ninth upshift into AUTO mode, the engine will be caused to synchronize for the required main and splitter clutch engagement.

[0047] In the current example, continuing operation in the AUTO mode is confirmed when either:

- (1) the confirmed gear ratio is an AUTO mode ratio (*i.e.*, ninth or tenth), and
- (2) vehicle speed exceeds the first reference value ($OS^*GR_{ENTRY} \geq$ the expected manual upshift RPM from the entry gear);

OR

an AUTO mode shift (ninth-tenth, tenth-ninth) is in progress.

[0048] Upon sensing that a shift from AUTO mode has occurred, the controller 124 will cause solenoid driver 132 to deactivate both solenoids to return splitter control to the operator. In the current example, a non-AUTO mode condition is confirmed when either:

- (1) an AUTO mode shift is not in progress, and
- (2) vehicle speed is less than a second reference value (REF_2), followed by
- (3) a shift into neutral;

OR

- (1) an AUTO shift is in progress, and
- (2) after a given period of time, engagement in an AUTO mode ratio cannot be confirmed;

OR

engagement in a non-AUTO mode ratio is confirmed.

[0049] The first, immediately preceding example involves a downshift out of AUTO mode, while the second example involves an apparent operator shift to main section neutral during an AUTO mode shift event.

[0050] In causing synchronous conditions for engagement of a target gear ratio, the engine is commanded to assume a rotational speed equal to true synchronous speed ($ES = OS^*GR_T$) plus or minus an offset value X equal to about 30 to 50 RPM. Accordingly, the engine is alternately commanded to a speed ($ES = (OS + X)^*GR_T$), and then a speed ($ES = (OS - X)^*GR_T$).

[0051] To confirm engagement/non-engagement, the value of ES/OS is compared over a period of time to known gear ratios plus or minus a given percent Y (*such as 0.5 to 1.5%*). Thus, by way of example, over a period of time, if $ES/OS = GR^*(1 \pm Y\%)$, then confirmation of engagement of GR is true. The offset X and the percentage error Y are selected so that at $ES = (OS + X)^*GR_T$, or at $ES = (OS - X)^*GR_T$, ES/OS will not equal $GR^*(1 \pm$

$Y\%)$.

[0052] The foregoing, as discussed in aforementioned co-pending EP-A-805 062 allows the use of speed signals to confirm engaged and neutral conditions without false readings due to engine synchronizing.

[0053] To confirm disengagement (of the entry gear ratio or of one of the AUTO mode ratios), the quotient of ES/OS is compared to the numerical value of the disengaging gear, plus or minus a disengaging gear error value, which may exceed the magnitude of the gear error value used to confirm engagement. For example, the disengaging gear error value may equal 1.5%, while the engaging gear error value may equal 1%.

[0054] Additionally, the gear error value used for confirming disengagement may be set larger on the positive side of synchronous of the disengaging gear than on the negative side to minimize false indications of neutral. Speed separations while still in gear tend to be higher on the positive side of synchronous due to the higher driving torque (the engine driving the vehicle tends to produce a greater positive torque magnitude than the negative torque produced when coasting with the vehicle driving the engine). Providing a larger $Pos_{Disengage_Gear_Error}$ and a smaller $Neg_{Disengage_Gear_Error}$ allows for protection against false indications of neutral on the positive side caused by aggressive throttle application, while still providing for a quick confirmation of neutral in the negative direction (the direction in which neutral is confirmed on most shifts).

[0055] In the preferred embodiment, the calculated gear ratio, ES/OS , is compared to an expanding window of error values and will be confirmed as disengaged only if it continues to remain outside the window. In the current example (see Figure 6), the calculated gear ratio must fall outside a range from:

[Engaged $GR^*(1 + (40^*\text{Counter}^*\text{Loop_Time}^*\text{Neg}_{Disengage_Gear_Error}))$]

to

[Engaged $GR^*(1 + (40^*\text{Counter}^*\text{Loop_Time}^*\text{Pos}_{Disengage_Gear_Error}))$],

where Counter is incremented by one each time this is true and decremented each time this is not true (minimizing at a value of 1). Disengagement is confirmed when the Counter reaches or exceeds a value equal to ($Synch_{Disengage_Time}/\text{Loop_Time}$). In the preferred embodiment, the values of $\text{Neg}_{Disengage_Gear_Error} = 1\%$, $\text{Pos}_{Disengage_Gear_Error} = 1.5\%$, and the maximum value of ($40^*\text{Counter}^*\text{Loop_Time}$) = 6.

[0056] The advantage of this "expanding window" over a fixed error band (prior art) is that it allows disengagement confirmation to start sooner (using the relatively small initial error window) while simultaneously providing better protection against false confirmations of neutral (using the relatively large, fully expanded window before confirming). If the calculated gear ratios fall

back within the window during the disengagement confirmation process, the window will decrement to the next smaller value (or to the smallest window) and upon the calculated gear ratio falling outside the window, the disengagement process will continue. The advantage gained with this "contracting window" over immediately resetting to the smallest error window is that it maintains a quick confirmation of true disengagement even if one data point falls inside the expanding error bounds, while preventing false neutral confirmation with transient speed separations induced by large torque oscillations.

[0057] Upon an electrical power failure, the solenoid-controlled valves will return to the open positions thereof, fluidly connecting conduits 108 and 110, and allowing manual selection of all ten forward ratios. Upon the solenoid driver detecting conditions indicative of a failure at one or both solenoids, the controller will cause both solenoids to be de-energized again, causing the two valves 134 and 136 to assume the open positions thereof, and allow manual selection of all ten forward ratios.

[0058] The control valve assembly 94, thus, provides a control allowing both manual and automatic splitter shifting, provides a favorable failure mode and as a module requires only four additional fluid connections (conduit 108 to port 138, conduit 110 to port 148, source S to port 146 and exhaust E_X to port 144) to the normally utilized manual splitter control.

[0059] As used herein, "main section" ratio positions will include the 1/2, 2/3, 3/4, 5/6, 7/8 and 9/10(A) ratio positions, and the range section is considered a portion of the manually shifted main section.

[0060] In the event of a failure in operating solenoids, in the splitter actuators, in the devices providing signals (ES, OS) indicative of engine and/or output shaft rotational speeds or the like, the preferred degraded mode is operation as a totally manual 10-speed splitter-type transmission, as illustrated in Figures 1 and 2.

[0061] When in the AUTO mode, upon sensing an actuator or a solenoid or a speed sensor fault or the like, the transmission is retained in its currently engaged splitter ratio until main section neutral can be confirmed, and then the splitter valve assembly 94 is returned to manual control. The control principle is not to go from an engaged splitter ratio to possible splitter neutral until the system is sure the operator has manually shifted into neutral. This will assure no unintended neutral conditions, although the system may drive as a wide-step 5-speed (*i.e.*, only 1-3-5-7-9 or 2-4-6-8-10 available) until neutral can be confirmed.

[0062] Accordingly, it may be seen that an improved compound transmission and shift control unit has been provided.

Claims

1. A method for controlling an automated mechanical transmission system which transmission system

comprises:

- 5 a manually shifted main section (12) having an input shaft (18) driven by a fuel-controlled engine, and
- 10 a splitter section (14) having an output shaft (58) and a splitter section actuator (86), whereby said splitter section actuator (86) is responsive in
- a manually shifted mode to manually supplied command signals and
- an automatic mode of operation to controller-supplied command signals to control shifting of said splitter section (14),

20 said method comprising the step of sensing values of input signals, including signals indicative of input and output shaft rotational speeds, said signals also being used to determine the existence of system faults;

said method being characterized by the further step:

25 upon sensing a system fault when in the automatic mode of operation, maintaining the currently engaged splitter ratio until a neutral condition is sensed in said main section (12) and, upon sensing said neutral condition, causing said splitter section actuator (86) to be controlled only by said manually supplied command signals.

- 30
2. The method of claim 1 wherein said system operates in said automatic mode of operation only in certain main section ratios.
 3. The method of claim 1 wherein said splitter section actuator comprises at least one solenoid-controlled valve responsive to said manually supplied control signals.
 - 40 4. A machine for controlling an automated mechanical transmission system which transmission system comprises:

45

a manually shifted main section (12) having an input shaft (18) driven by a fuel-controlled engine, and

a splitter section (14) having an output shaft (58) and a splitter section actuator (86), whereby said splitter section actuator (86) is responsive in

- a manually shifted mode to manually supplied command signals and
- an automatic mode of operation to controller-supplied command signals to control

shifting of said splitter section (14), and

logic elements sensing values of input signals, including signals indicative of input and output shaft rotational speeds, said signals also being used to determine the existence of system faults; **the machine being characterized by**

logic elements effective, upon sensing a system fault when in the automatic mode of operation, maintaining the currently engaged splitter ratio until a neutral condition is sensed in said main section (12) and, upon sensing said neutral condition, causing said splitter section actuator (86) to be controlled only by said manually supplied command signals.

5. The machine of claim 4 wherein said system is designed to operate in said automatic mode of operation only in certain main section ratios.
6. The machine of claim 4 wherein said splitter section actuator comprises at least one solenoid-controlled valve responsive to said manually supplied control signals.

Betriebes in dem automatischen Modus die gegenwärtig eingelegte Split-Gangstufe aufrecht zu erhalten, bis in der Hauptgetriebegruppe (12) eine Leerlaufbedingung erfasst wird, und bei Erfassen dieser Leerlaufbedingung zu veranlassen, dass der Splitgruppenaktuator (86) lediglich durch die manuell bereitgestellten Steuerbefehle gesteuert wird.

10. 2. Verfahren nach Anspruch 1, bei dem das System lediglich in gewissen Gangstufen der Hauptgetriebegruppe in dem automatischen Betriebsmodus arbeitet.
15. 3. Verfahren nach Anspruch 1, bei dem der Splitgruppenaktuator wenigstens ein elektromagnetisch gesteuertes Ventil enthält, das in Abhängigkeit von den manuell erzeugten Steuersignalen arbeitet.
20. 4. Vorrichtung zum Steuern/Regeln eines automatisierten mechanischen Getriebesystems, wobei zu dem Getriebesystem gehören:

eine manuell geschaltete Hauptgetriebegruppe (12) mit einer Eingangswelle (18), die mittels eines über die Treibstoffzufuhr gesteuerten/ge- regelten Motors angetrieben ist, und eine Splitgruppe (14) mit einer Ausgangswelle (58) und einem Splitgruppenaktuator (86), wo- bei der Splitgruppenaktuator (86)

- in einem manuell geschalteten Modus auf manuell bereitgestellte Steuerbefehle und
- in einem automatischen Betriebsmodus auf von einem Controller gelieferte Steuer- befehle zur Steuerung des Schaltens der Splitgruppe (14) anspricht, und

Logikelemente, die dazu dienen, Werte von Eingangssignalen zu erfassen, zu denen Signale gehören, die für die Drehzahlen der Eingangs- und Ausgangswelle kennzeichnend sind, wobei die Signale außerdem dazu verwendet werden, um die Existenz von Systemfehlern zu erfassen; **wobei die Vorrichtung gekennzeichnet ist durch**

Logikelemente, die dazu dienen, bei Erfassen eines während eines Betriebes in dem automatischen Modus auftretenden Systemfehlers die gegenwärtig eingelegte Split-Gangstufe aufrecht zu erhalten, bis in der Hauptgetriebegruppe (12) eine Leerlaufbedingung erfasst ist, und bei Erfassen dieser Leerlaufbedingung zu veranlassen, dass der Splitgruppenaktuator (86) lediglich durch die manuell bereitgestellten Steuerbefehle geregelt/ges- steuert wird.

5. Vorrichtung nach Anspruch 4, bei der das System dergestalt konstruiert ist, dass es lediglich in gewis-

Patentansprüche

1. Verfahren zur Steuerung/Regelung eines automatisierten mechanischen Getriebesystems, wobei zu dem Getriebesystem gehören:

eine manuell geschaltete Hauptgetriebegruppe (12) mit einer Eingangswelle (18), die mittels eines über die Treibstoffzufuhr gesteuerten/ge- regelten Motors angetrieben wird, und eine Splitgruppe (14) mit einer Ausgangswelle (58) und einem Splitgruppenaktuator (86), wo- bei der Splitgruppenaktuator (86)

- in einem manuell geschalteten Modus auf manuell bereitgestellte Steuerbefehle und
- in einem automatischen Betriebsmodus auf von einem Controller gelieferte Steuer- befehle zur Steuerung des Schaltens der Splitgruppe (14) anspricht,

wobei zu dem Verfahren der Schritt gehört, Werte von Eingangssignalen zu erfassen, zu denen Signale gehören, die für die Drehzahlen der Eingangs- und Ausgangswelle kennzeichnend sind, wobei die Signale außerdem dazu verwendet werden, um das Vorhandensein von Systemfehlern zu erfassen;

wobei das Verfahren gekennzeichnet ist durch den zusätzlichen Schritt:

bei Erfassen eines Systemfehlers während des

- sen Gangstufen der Hauptgetriebegruppe in dem automatischen Betriebsmodus arbeitet.
6. Vorrichtung nach Anspruch 4, bei der der Splitgruppenaktuator wenigstens ein elektromagnetisch gesteuertes Ventil enthält, das in Abhängigkeit von den manuell bereitgestellten Steuersignalen arbeitet.
- Revendications
1. Procédé pour commander un système de transmission mécanique automatisé, lequel système de transmission comprend :
- une section principale (12) à changement de rapport manuel ayant un arbre d'entrée (18) entraîné par un moteur commandé par le carburant et,
 - une section de division (14) ayant un arbre de sortie (58) et un actionneur de section de division (86), dans lequel ledit actionneur de section de division (86) commande le changement de rapport de ladite section de division (14) en réponse
- à des signaux d'ordre transmis manuellement dans un mode à changement manuel,
 - et à des signaux d'ordre transmis par un contrôleur dans un mode de fonctionnement automatique,
- ledit procédé comprenant la phase consistant à détecter des valeurs de signaux d'entrée, y compris des signaux indicatifs de vitesses de rotation des arbres d'entrée et de sortie, lesdits signaux étant aussi utilisés pour déterminer l'existence de défauts du système ;
- ledit procédé étant caractérisé par la phase additionnelle suivante :
- en réponse à la détection d'un défaut du système alors qu'il est dans le mode de fonctionnement automatique, maintenir le rapport de division engagé actuellement jusqu'à ce qu'un état de point mort soit détecté dans ladite section principale (12) et, en réponse à la détection du dit état de point mort, faire en sorte que ledit actionneur (86) de la section de division soit commandé uniquement par lesdits signaux d'ordre transmis manuellement.
2. Procédé selon la revendication 1, dans lequel ledit système n'opère dans ledit mode de fonctionnement automatique que dans certains rapports de la section principale.
3. Procédé selon la revendication 1, dans lequel ledit actionneur de la section de division comprend au moins une soupape commandée par électroaimant qui répond auxdits signaux de commande transmis manuellement.
4. Machine pour commander un système de transmission mécanique automatisé, lequel système de transmission comprend :
- une section principale (12) à changement de rapport manuel ayant un arbre d'entrée (18) entraîné par un moteur commandé par le carburant et,
 - une section de division (14) ayant un arbre de sortie (58) et un actionneur de section de division (86), dans laquelle ledit actionneur de section de division (86) commande le changement de rapport de ladite section de division (14) en réponse
 - à des signaux d'ordre transmis manuellement dans un mode à changement manuel,
 - et à des signaux d'ordre transmis par un contrôleur dans un mode de fonctionnement automatique, et
- des éléments logiques qui détectent des valeurs de signaux d'entrée, y compris des signaux indicatifs de vitesses de rotation des arbres d'entrée et de sortie, lesdits signaux étant aussi utilisés pour déterminer l'existence de défauts du système ;
- la machine étant caractérisée en ce que en réponse à la détection d'un défaut du système alors qu'il est dans le mode de fonctionnement automatique, les éléments logiques maintiennent le rapport de division engagé actuellement jusqu'à ce qu'un état de point mort soit détecté dans ladite section principale (12) et, en réponse à la détection du dit état de point mort, ils font en sorte que ledit actionneur (86) de la section de division soit commandé uniquement par lesdits signaux d'ordre transmis manuellement.
5. Machine selon la revendication 4, dans laquelle ledit système est conçu pour n'opérer dans ledit mode de fonctionnement automatique que dans certains rapports de la section principale.
6. Machine selon la revendication 4, dans laquelle ledit actionneur de la section de division comprend au moins une soupape commandée par électroaimant qui répond auxdits signaux de commande transmis manuellement.

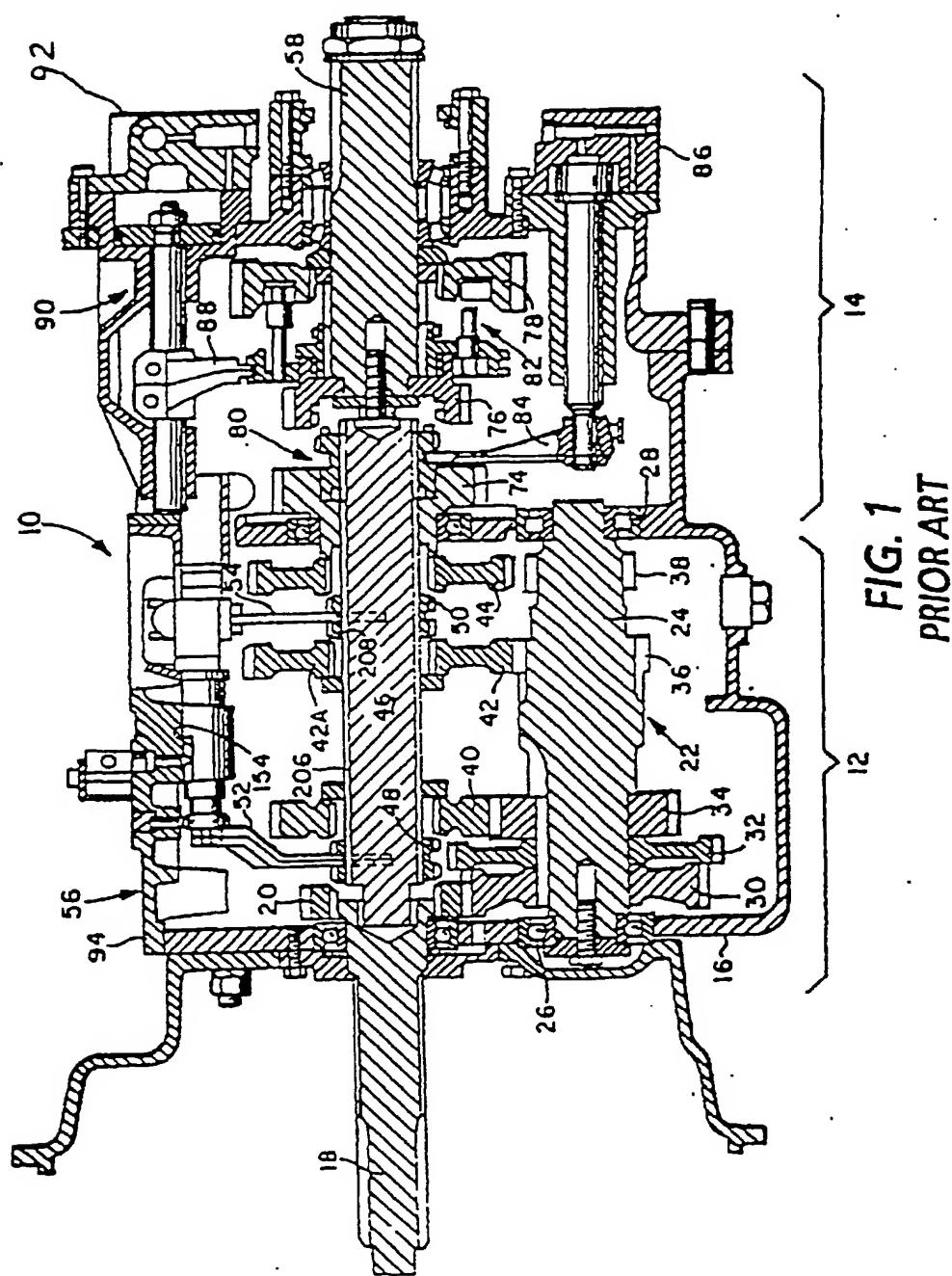


FIG. 1
PRIOR ART

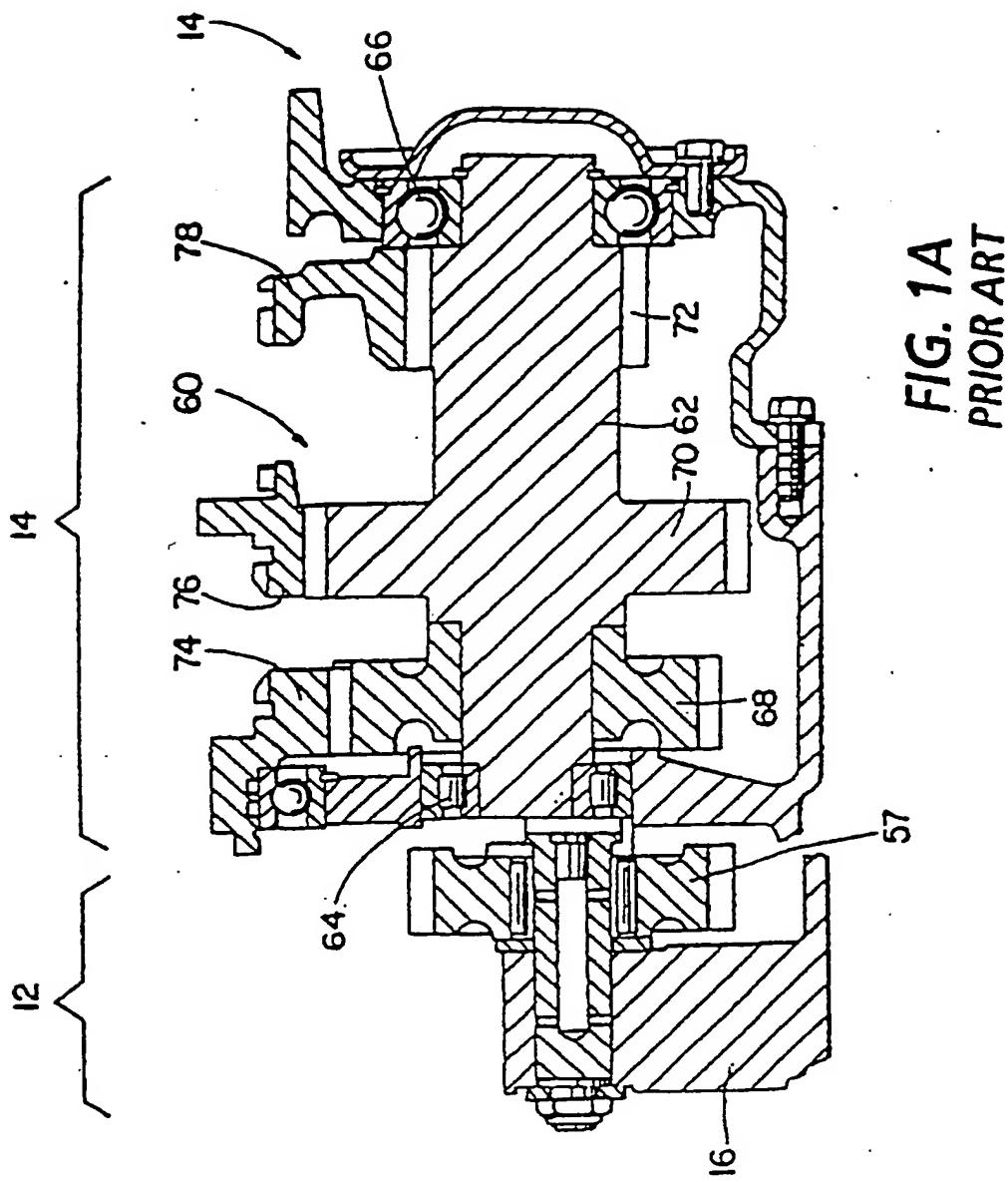


FIG. 1A
PRIOR ART

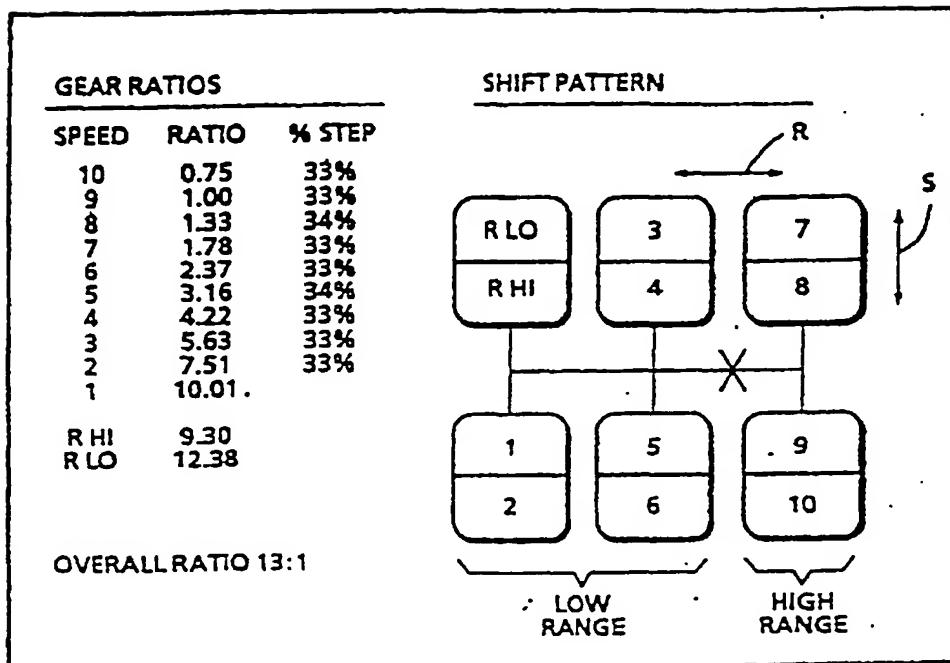
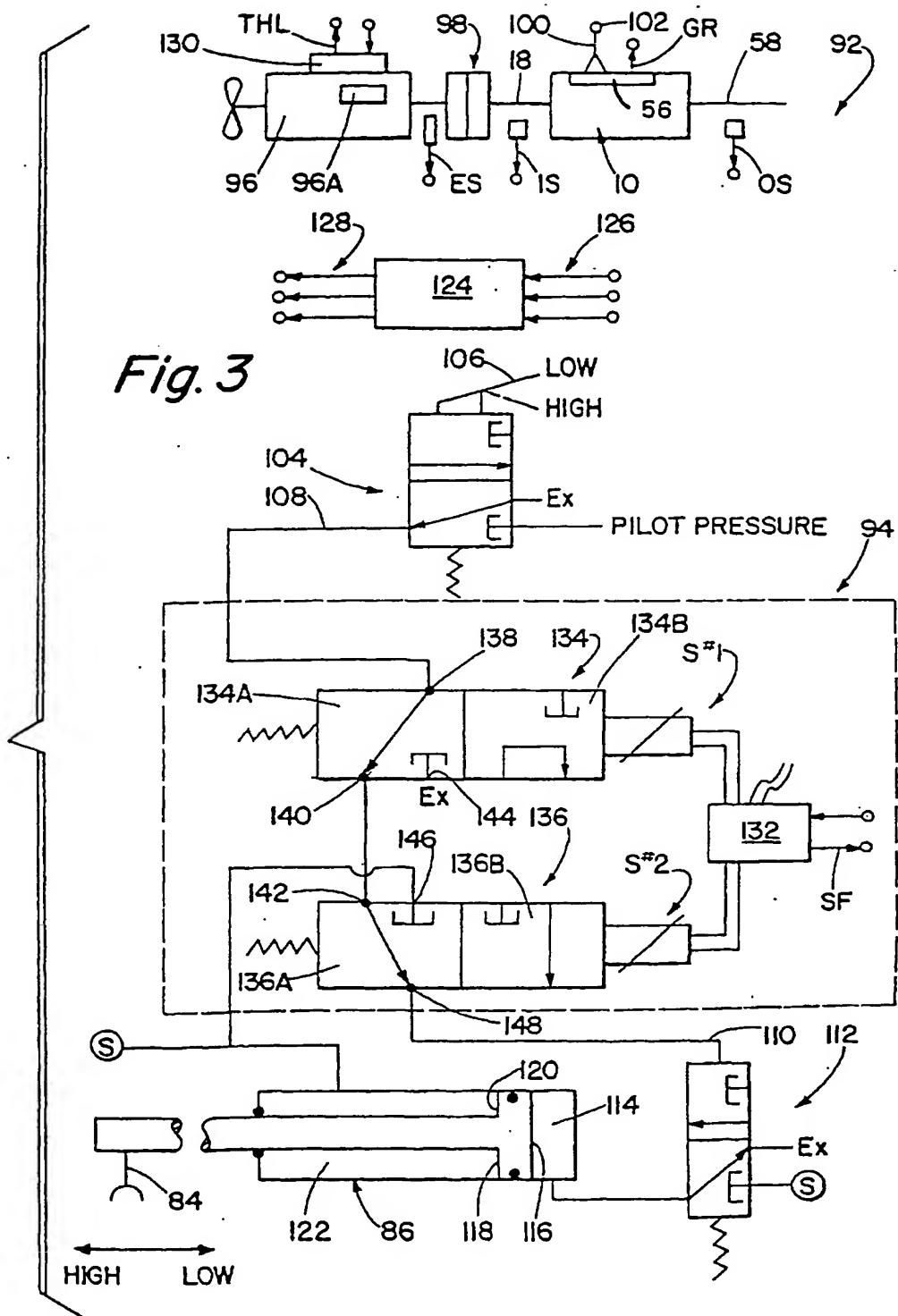


FIG. 2
PRIOR ART



VALVE TABLE

GEAR	S#1	S#2
1-8	OFF	OFF
9	ON	OFF
10	OFF/ON	ON

FIG 4.

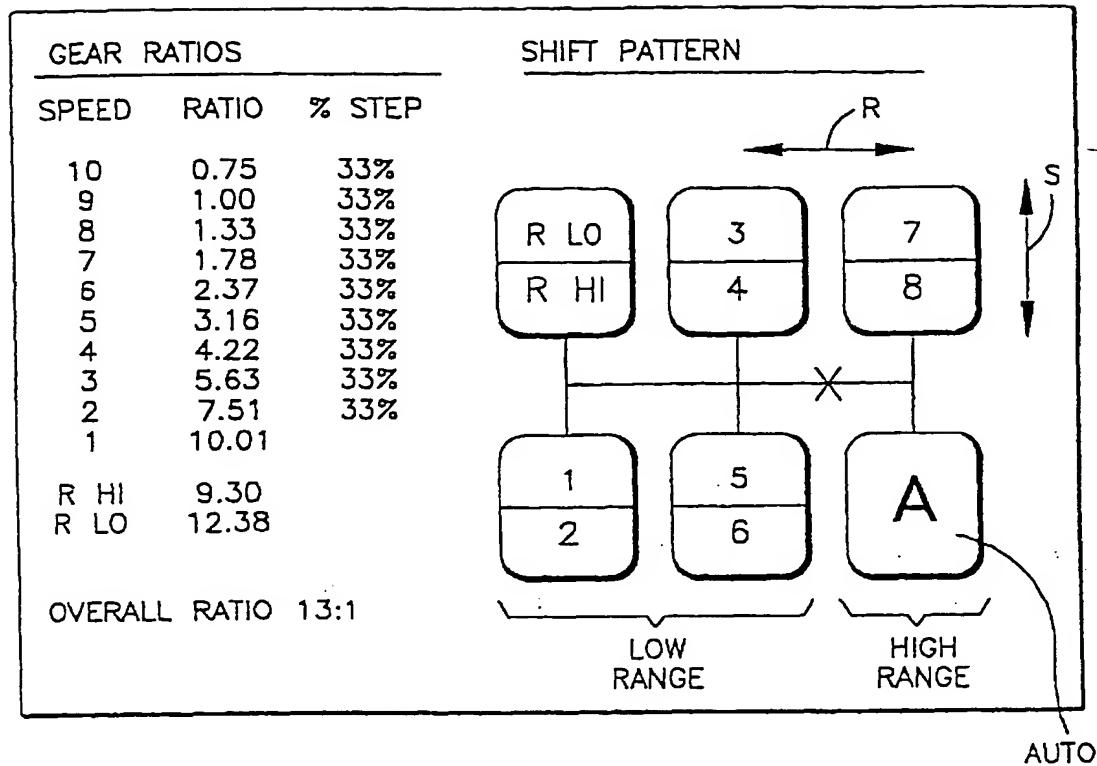


Fig.5

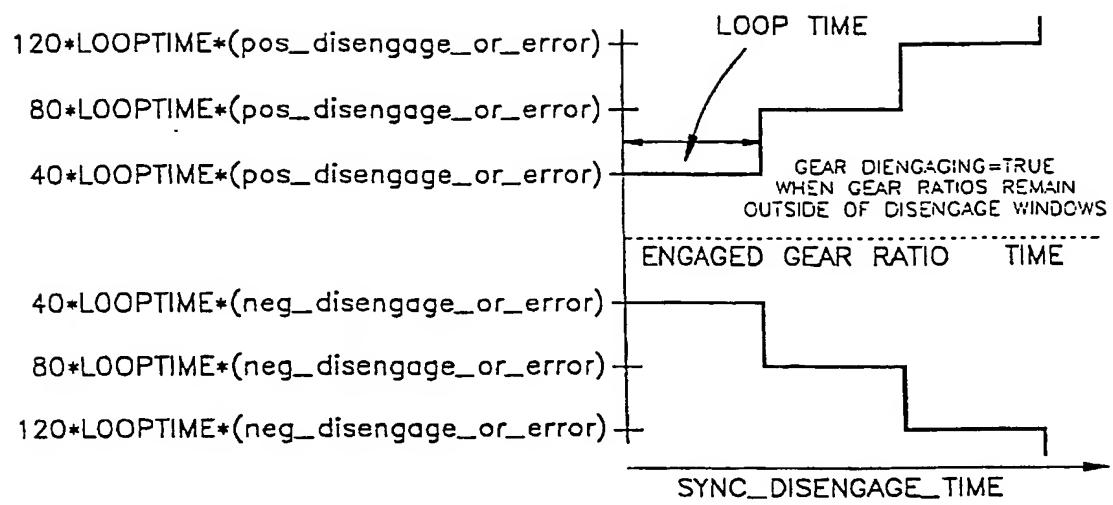


Fig.6

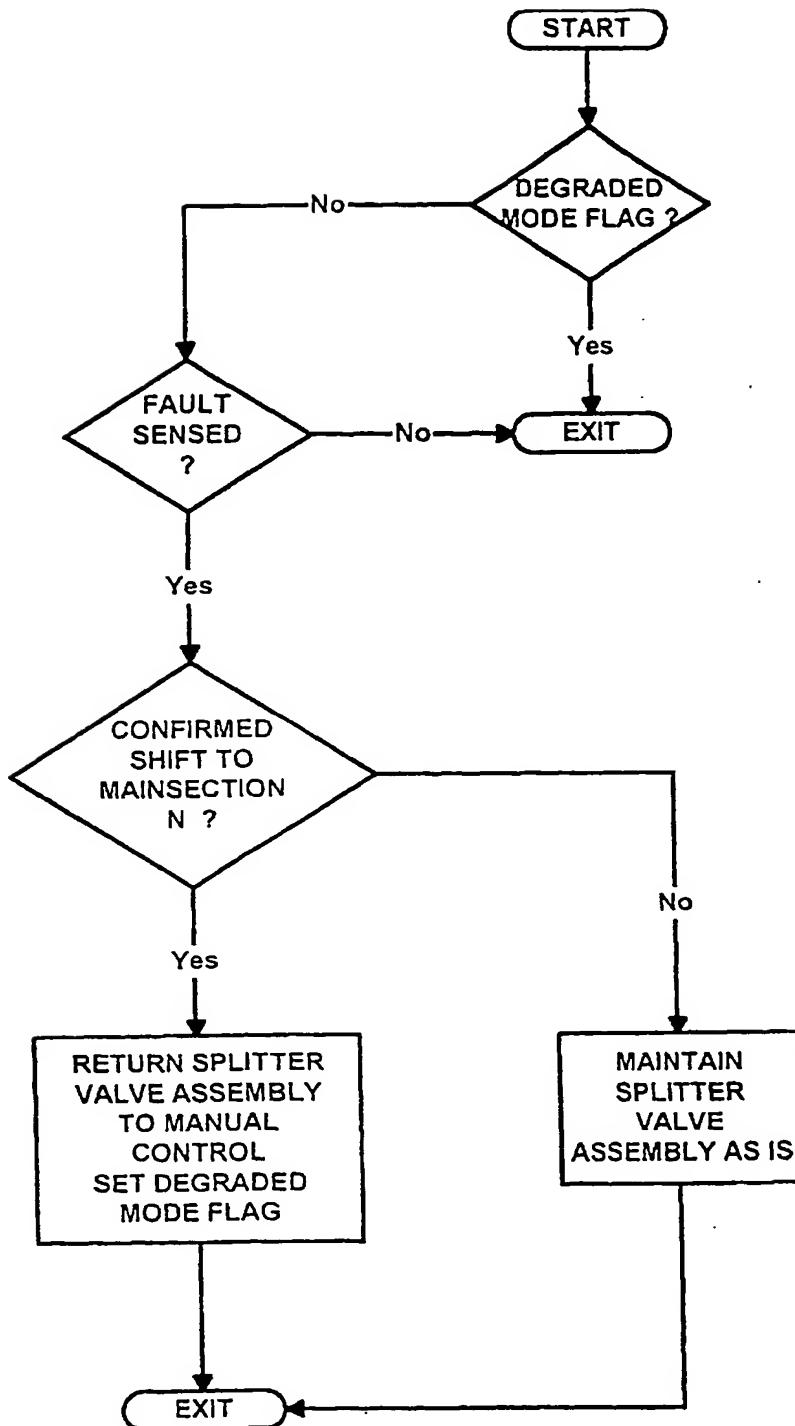


FIG. 7

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